

# Experiment

Be careful with  
the magnets!!  
They are very  
Strong!!!

Keep them away  
From your computer  
And credit cards

# 2.76 / 2.760 Lecture 3: Large scale

**Flexure experiment**

**Constraints**

**Micro-fabrication**

**Micro-physics scaling**

**Assignment**



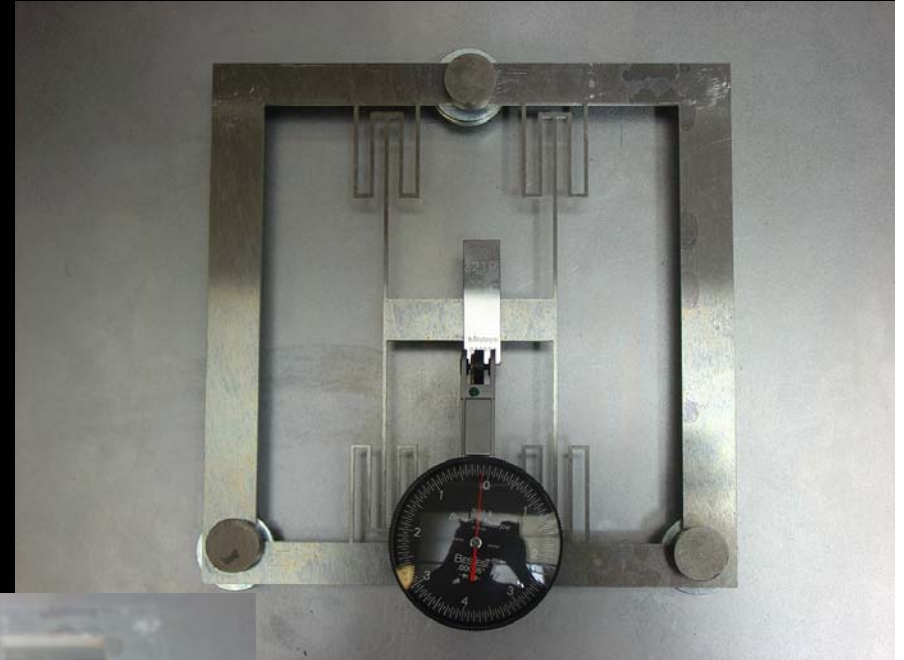
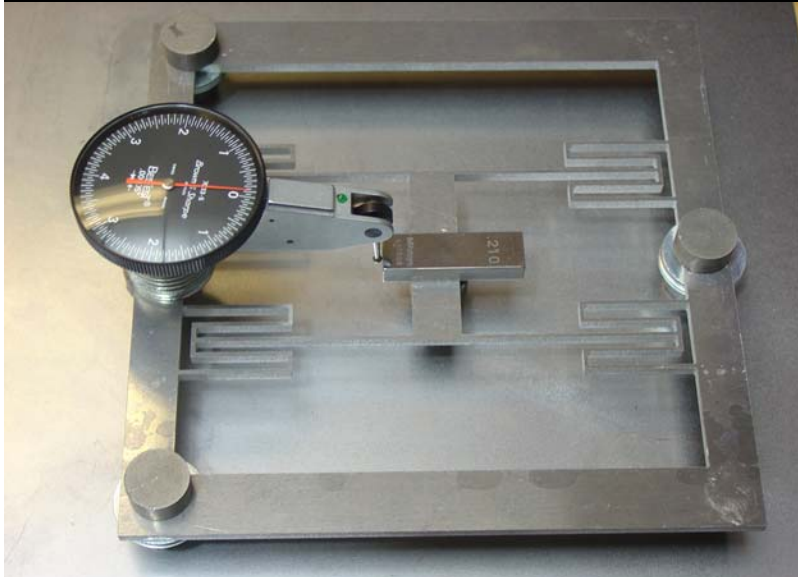
# Experiment

- (1) What is the smallest displacement you can “really” measure with the probes? It is smaller than the ticks....
- (2) What metrology/measurement issues must be dealt with?
- (3) Estimate the effect of actuator angular misalignment on parasitic error. Do an order of magnitude estimate. Use your finger...
- (4) How should you design a constraint between the actuator and the flexure to mitigate angular misalignment?
- (5) How effective would this constraint be? What are the important design variables? Use CoMeT...

**Time Limit: 30 minutes**

**Email results to me when time is called**

# Experiment



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# Discussion

**Metrology/measurement issues**

**Actuator angular misalignment on parasitic error**

**Effectiveness of constraint between actuator-flexure**

# Purpose of today

$$\begin{array}{c}
 O_{Macro} \\
 O_{Meso} \\
 O_{Micro} \\
 O_{Nano}
 \end{array}
 =
 \begin{array}{cccc}
 f_{11} \left( \begin{array}{c} SR_{Macro} \\ Macro \end{array} \right) & f_{12} \left( \begin{array}{c} SR_{Meso} \\ Meso \end{array} \right) & f_{13} \left( \begin{array}{c} SR_{Micro} \\ Micro \end{array} \right) & f_{14} \left( \begin{array}{c} SR_{Nano} \\ Nano \end{array} \right) \\
 f_{21} \left( \begin{array}{c} SR_{Macro} \\ Macro \end{array} \right) & f_{22} \left( \begin{array}{c} SR_{Meso} \\ Meso \end{array} \right) & f_{23} \left( \begin{array}{c} SR_{Micro} \\ Micro \end{array} \right) & f_{24} \left( \begin{array}{c} SR_{Nano} \\ Nano \end{array} \right) \\
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 \end{array}
 \cdot
 \begin{array}{c}
 I_{Macro} \\
 I_{Meso} \\
 I_{Micro} \\
 I_{Nano}
 \end{array}$$

Finish mechanical gain factors to make big machines work with little machines

Micro-scale flow/interface dominators

- Micro-scale fabrication
- Micro-scale surface/volume physics

# Constraints

# Constraint-based design

## Constraint-based compliant mechanism design

### STEP 1: Design requirements

Motion path, stiffness, load capacity, etc...

### STEP 2: Motion path decomposition

Arcs, lines, rotation pts. sub-paths

### STEP 3: Kinematic parametric concepts

Motions, constraint metric, symmetry, etc.

### STEP 4: Constraint-motion addition rules

Serial, parallel, hybrid

### STEP 5: Topology concept generation

Path & constraint driven

### STEP 6: Concept selection phase I

Path errors & over constraint

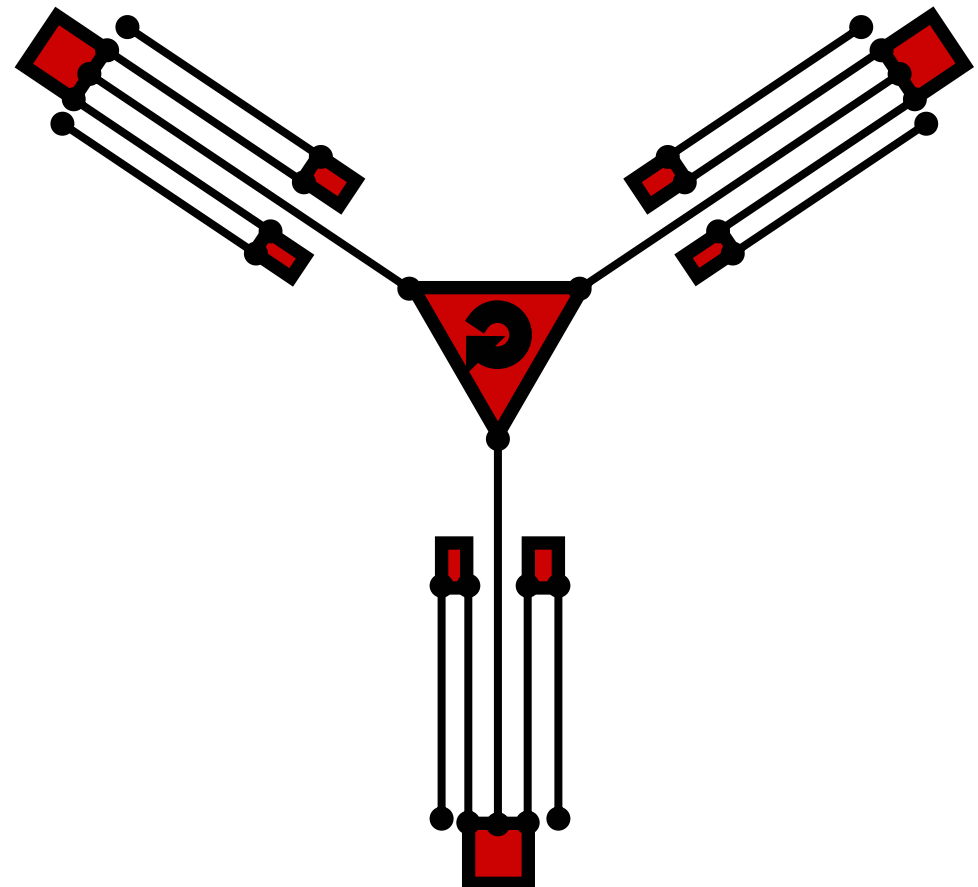
### STEP 7: Size and shape optimization

Stiffness, load capacity, efficiency, etc...

### STEP 8: Concept selection phase II

Direct comparison with design requirements

Photo removed for copyright reasons.  
Compliant test rig for automotive steering column.





# Exact constraint

**At some scale, everything is a mechanism**

## Exact constraint: Achieve desired motion

- By applying minimum number of constraints
- Arranging constraints in optimum topology
- Adding constraints only when necessary

**Visualization is critical, this is not cookbook**

### For now:

- Start with ideal constraints
- Considering small motions
- Constraints = lines

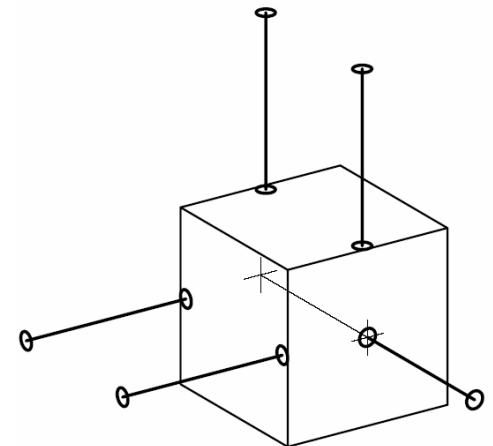


Figure: Layton Hales PhD Thesis, MIT.

# Constraint fundamentals

**Rigid bodies have 6 DOF**

**DOC = # of linearly independent constraints**

**DOF = 6 - DOC**

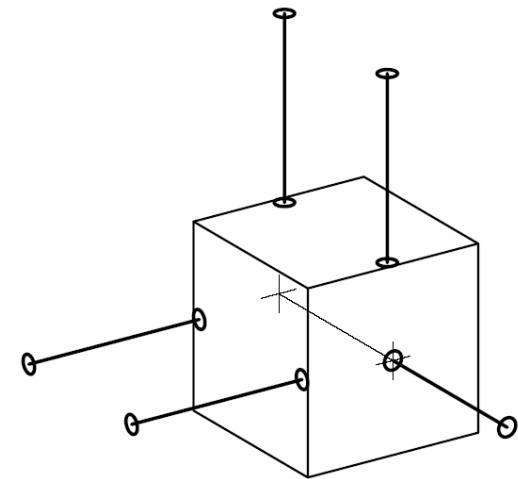


Figure: Layton Hales PhD Thesis, MIT.

**A linear displacement can be visualized as a rotation about a point which is “far” away**

# Statements

**Points on a constraint line move perpendicular to the constraint line**

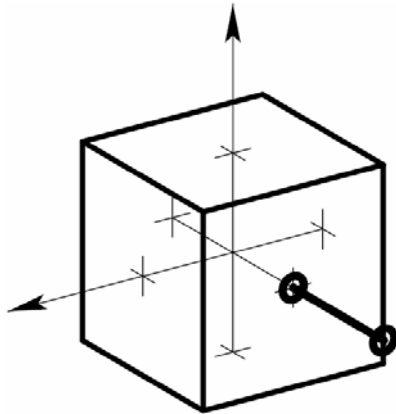
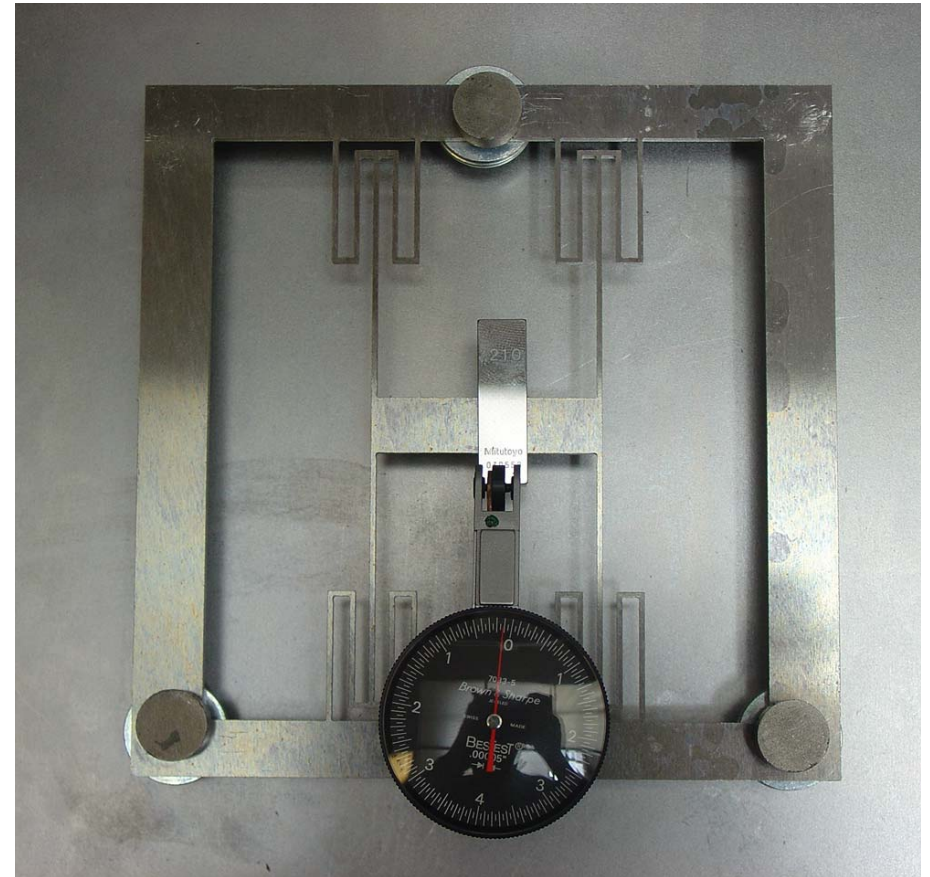


Figure: Layton Hales PhD Thesis, MIT.

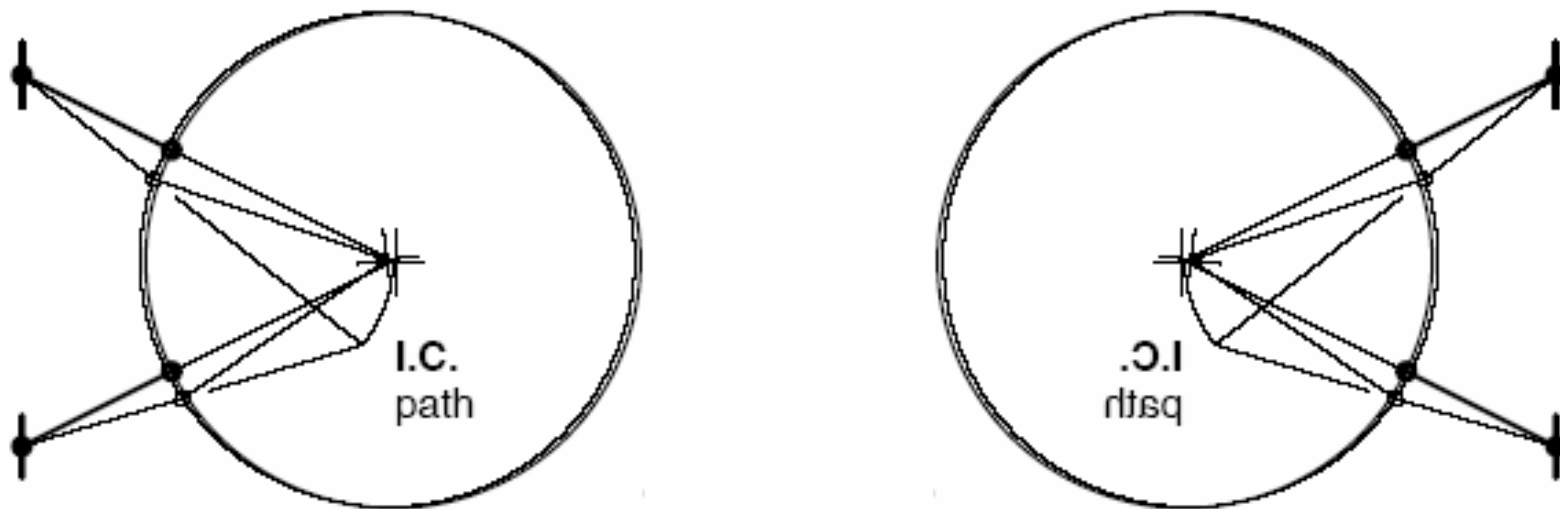
**Constraints along this line are equivalent**

Diagrams removed for copyright reasons.  
Source: Blanding, D. L. *Exact Constraint: Machine Design using Kinematic Principles*.  
New York: ASME Press, 1999.



# Statements

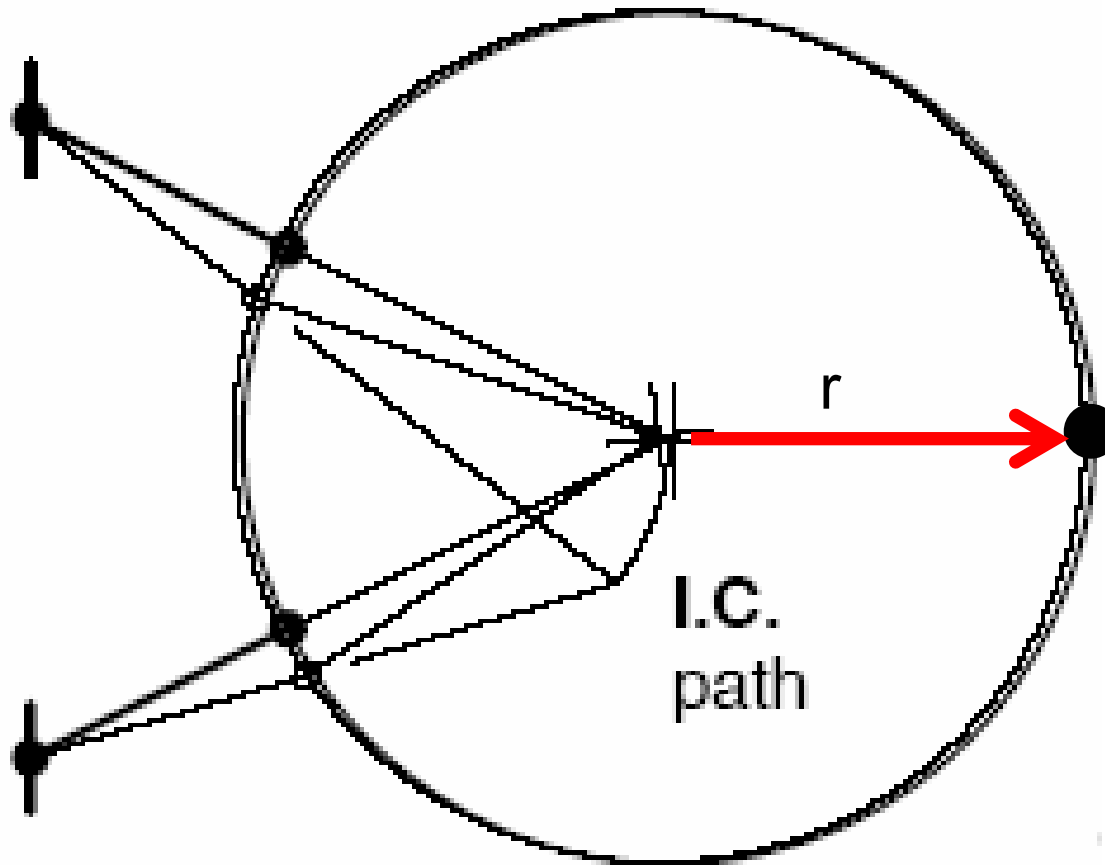
**Intersecting, same-plane constraints are equivalent to other same-plane intersecting constraints**



**Instant centers are powerful tool for visualization, diagnosis, & synthesis**

# Abbe error

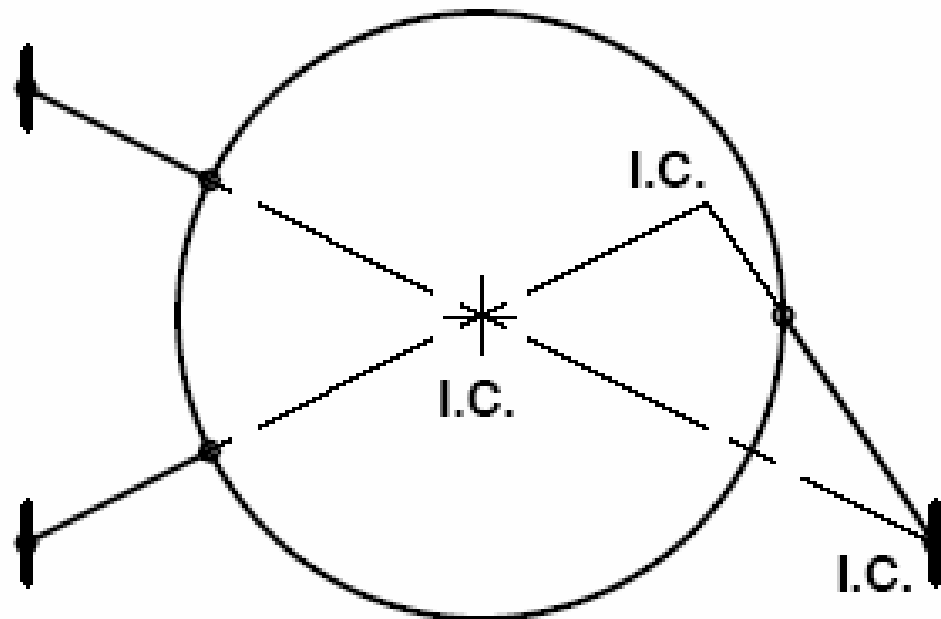
Error due to magnified moment arm



# Statements

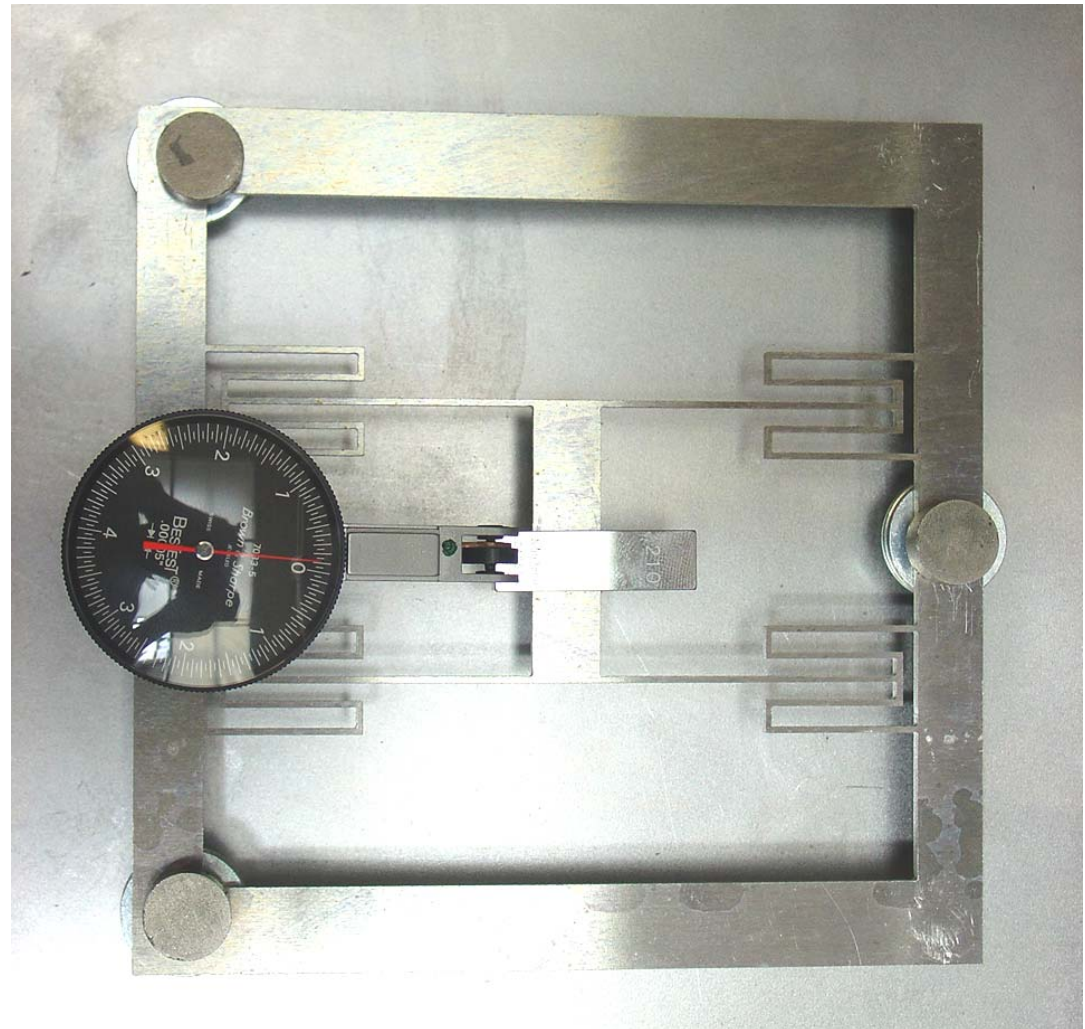
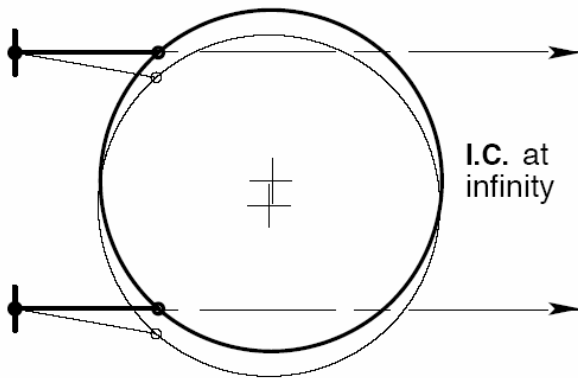
**Constraints remove rotational degree of freedom**

**Length of moment arm determines the quality of the rotational constraint**



# Statements

**Parallel constraints may be visualized/treated as intersecting at infinity**



# Basic elements

Bars

Beams

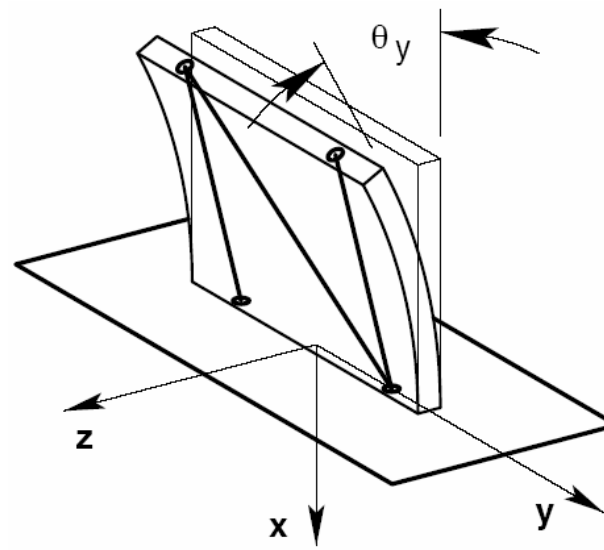
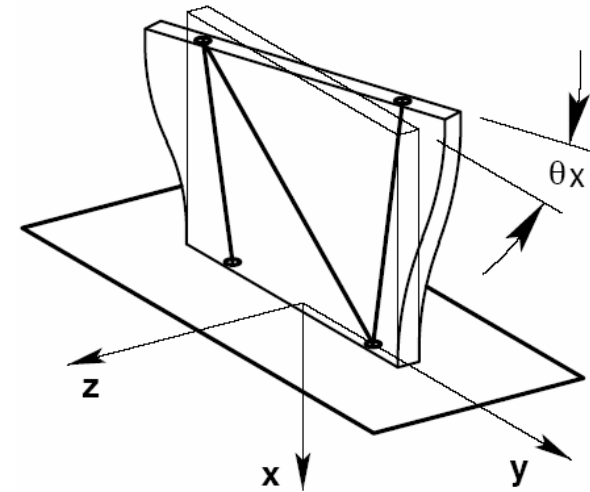
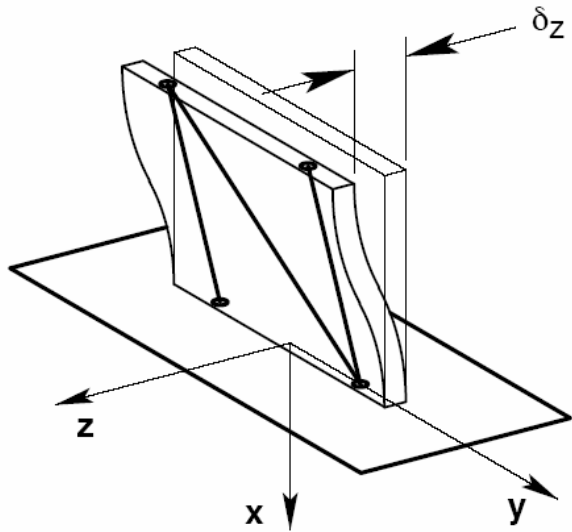
Plates

Diagrams removed for copyright reasons.  
Source: Blanding, D. L. *Exact Constraint:  
Machine Design using Kinematic Principles.*  
New York: ASME Press, 1999.

Notch Hinge



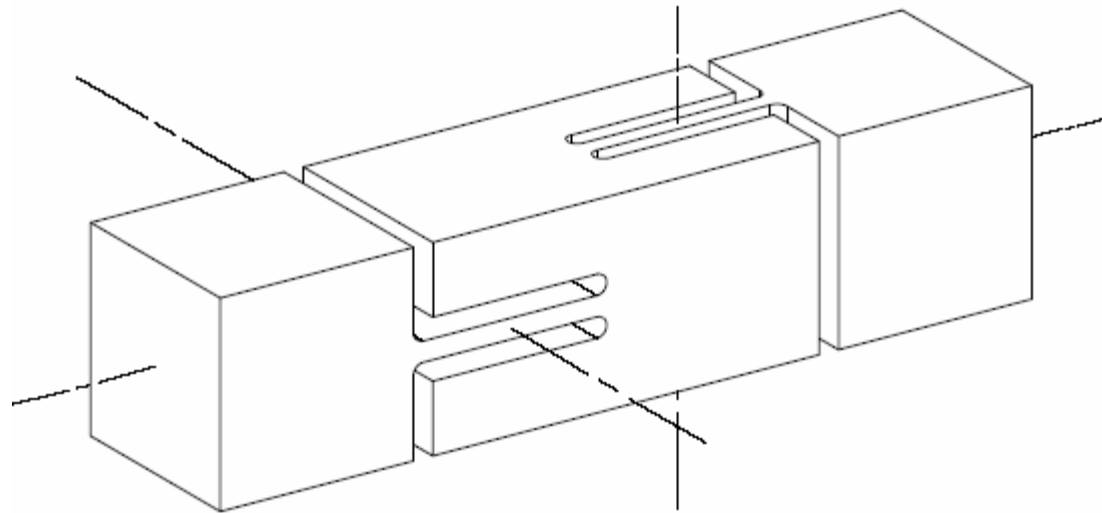
# Examples



Do you really get  $\delta z$ ?

Figures: Layton Hales PhD Thesis, MIT.

# Examples



Series: Add DOF

Follow the serial chain

Pick up every DOF

Differentiate series by  
Load path

Shared load path =  
Series

This could be 5 DOF

Depends on blade  
length

Figure: Layton Hales PhD Thesis, MIT.

# Examples

Parallel: Add Constraints

Where there is a common DOF,  
then have mechanism DOF

There are no conflicts in  
circumferential displacement  
To  $\theta_z$

Non-shared load paths = parallel

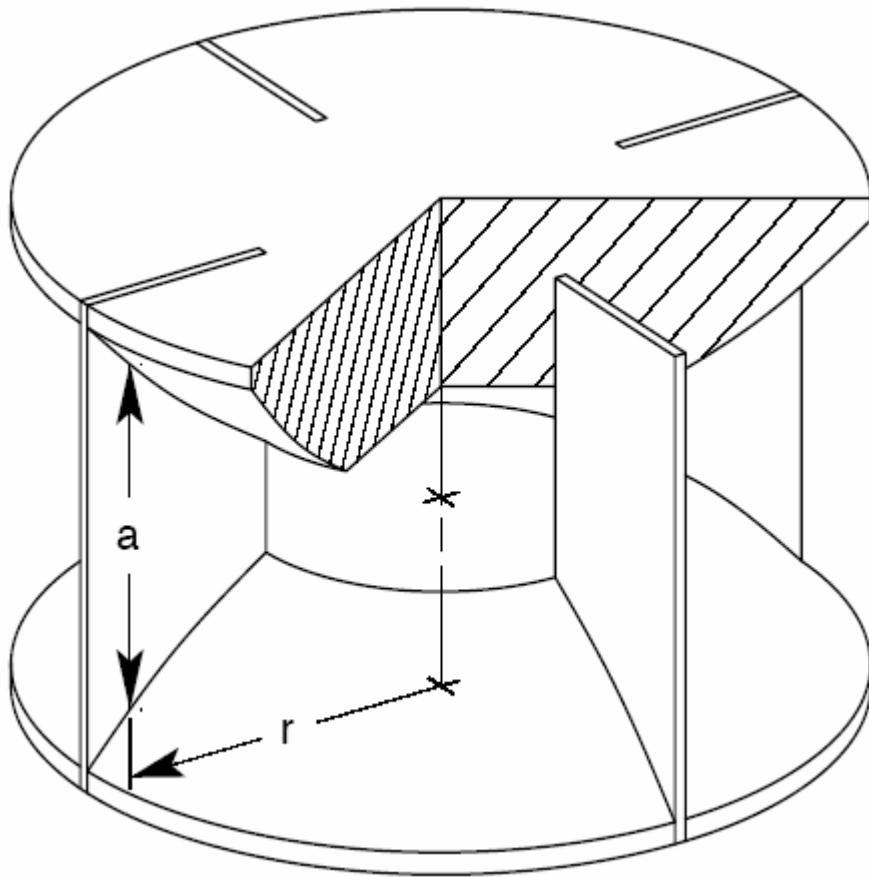


Figure: Layton Hales PhD Thesis, MIT.

# Examples

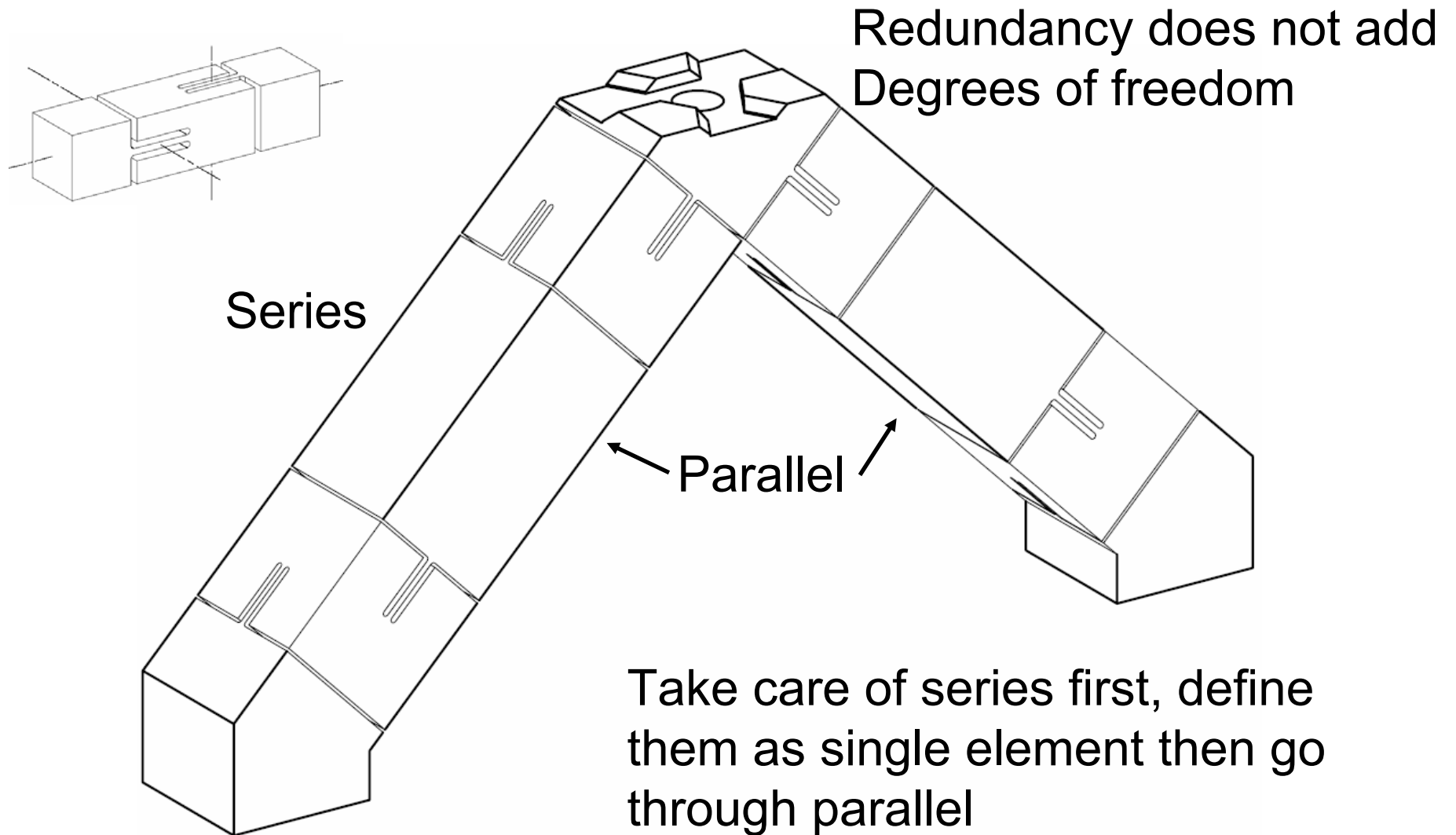
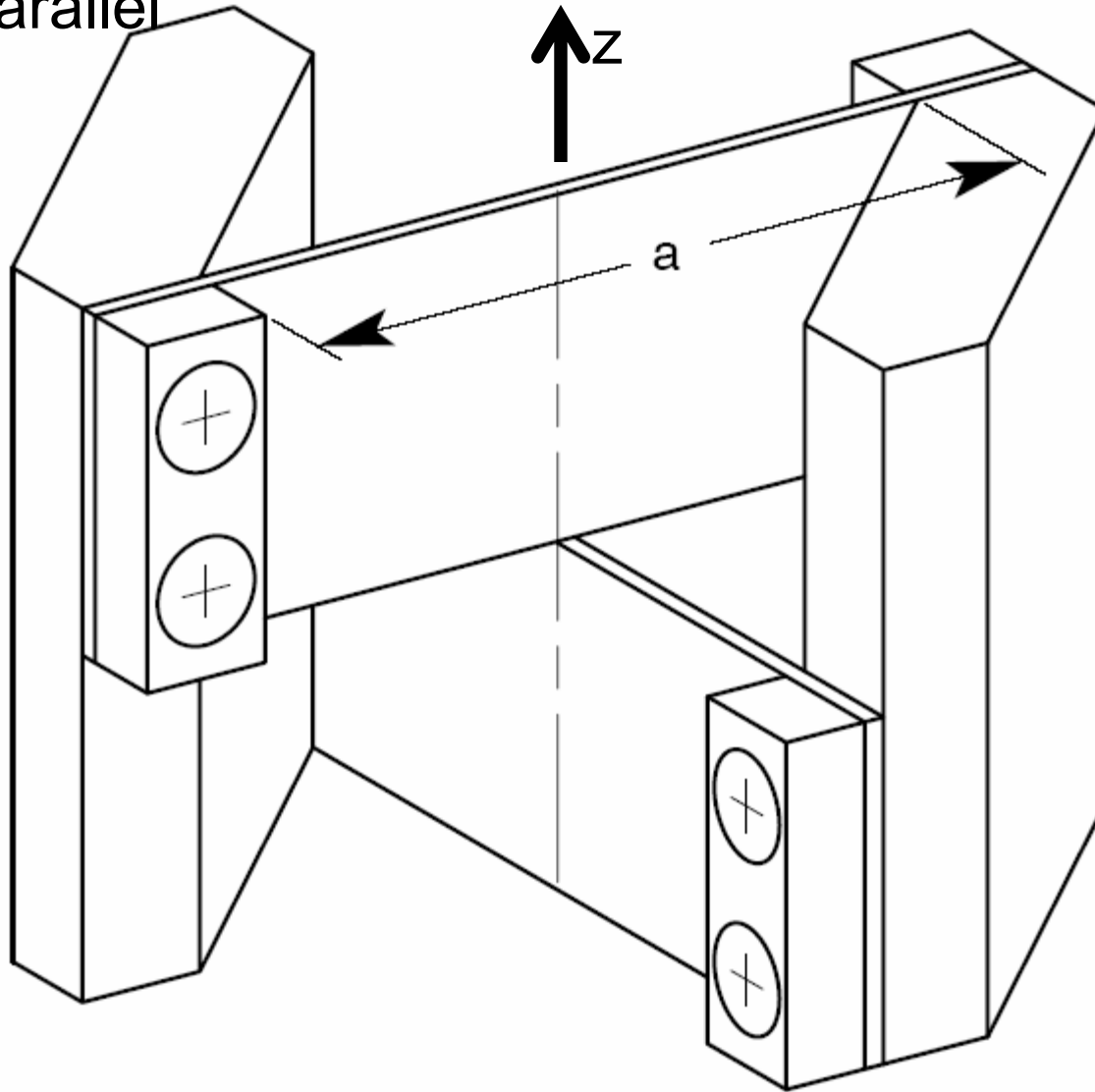


Figure: Layton Hales PhD Thesis, MIT.

# Examples

Parallel



Theta z is a common  
Degree of freedom

All others conflict

Figure: Layton Hales PhD Thesis, MIT.

# Examples

$\delta z$  is a common  
Degree of freedom

All others conflict

Rotation arms cause  
Conflict in out-of-plane  
rotations

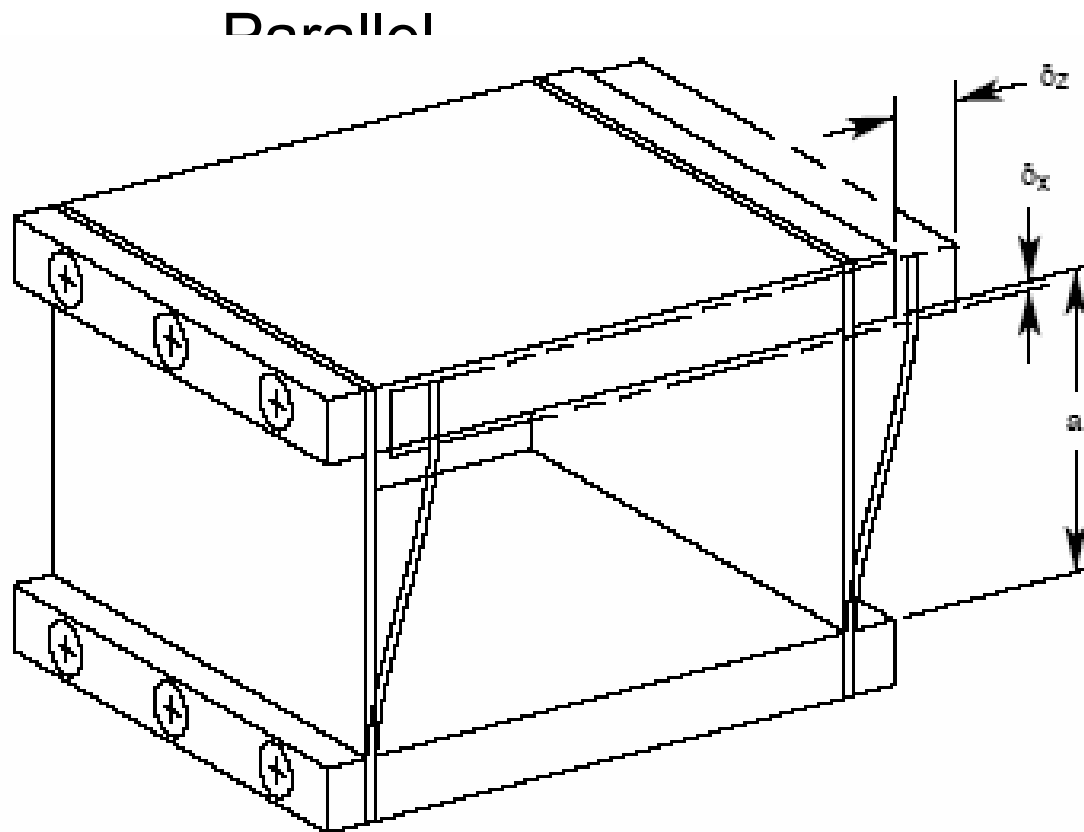


Figure: Layton Hales PhD Thesis, MIT.

# Over constraint

**Flexures are often forgiving of over constraint**

**Over constraint = redundant constraint**

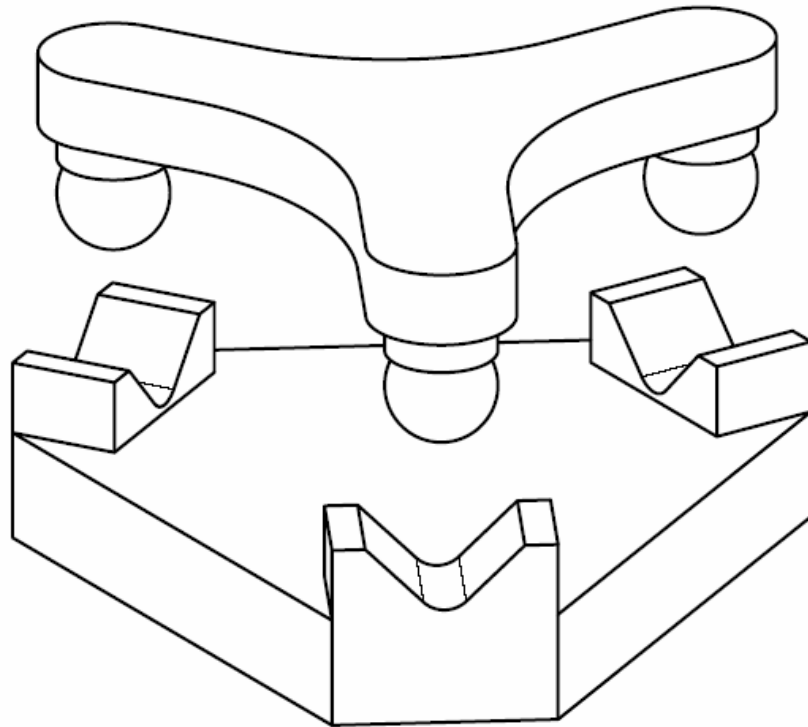
**Identifying over constraint**

□ How much energy is stored?

**General metric relating constraint stiffness to motion along constraint**

$$\frac{K_{\parallel}}{K_{\perp}} \cdot \frac{\delta_{\perp}}{\delta_{\parallel}} \rightarrow CM_k \cdot CM_{\delta} \ll 1$$

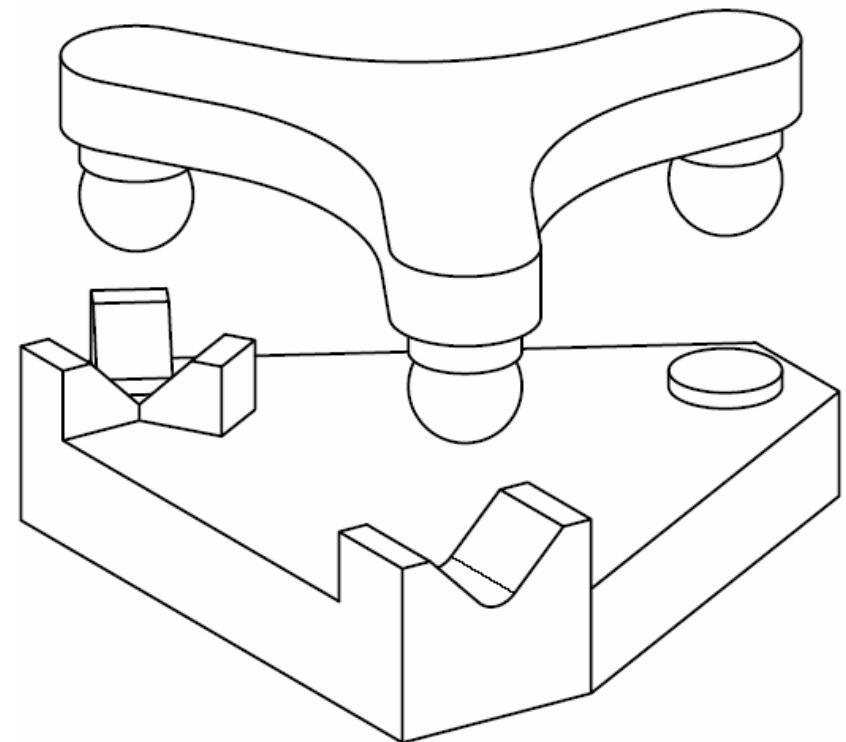
# Extension: Fixtures



Maxwell

You will need to build a Passive fixture for your STM

Kelvin



Figures: Layton Hales PhD Thesis, MIT.



# Fixtures as mechanisms

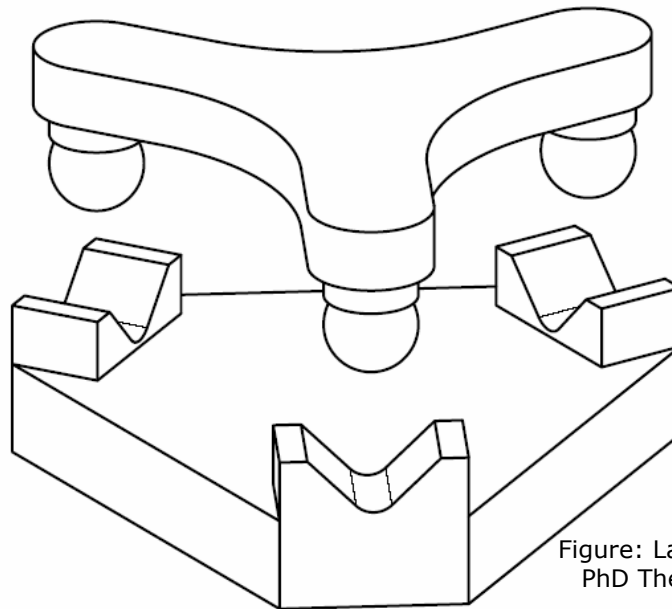
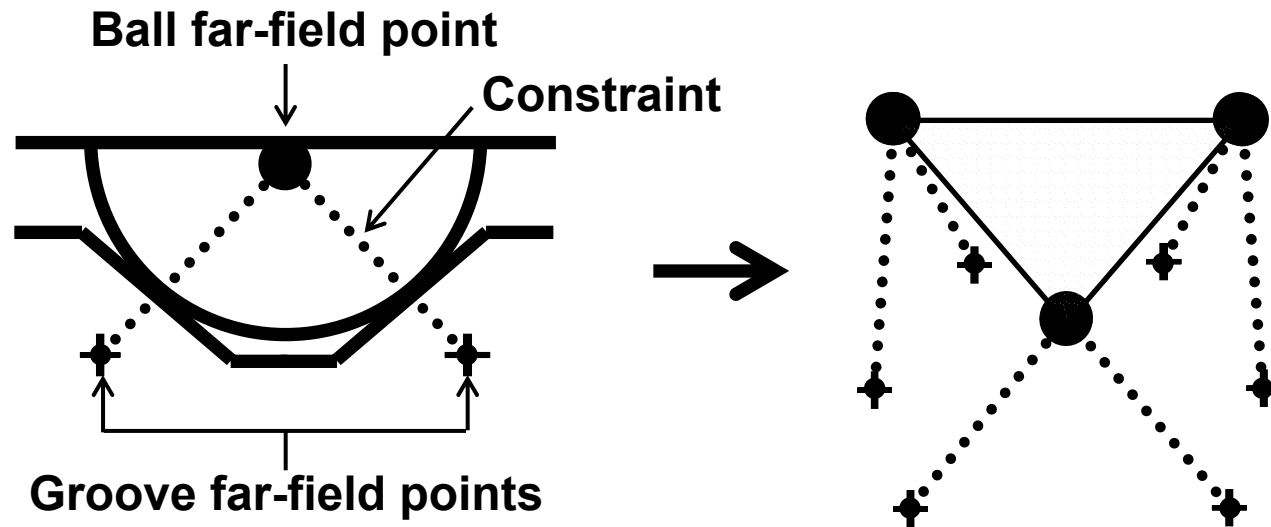


Figure: Layton Hales  
PhD Thesis, MIT.

# Details of QKC element geometry

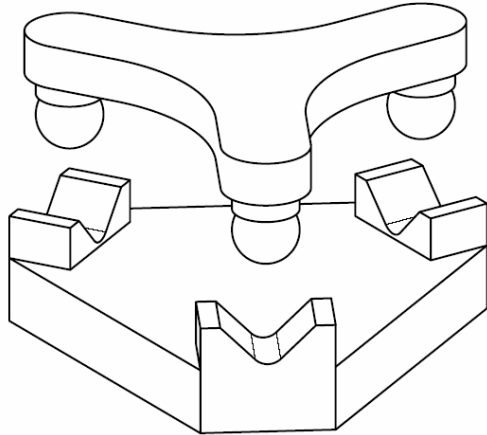
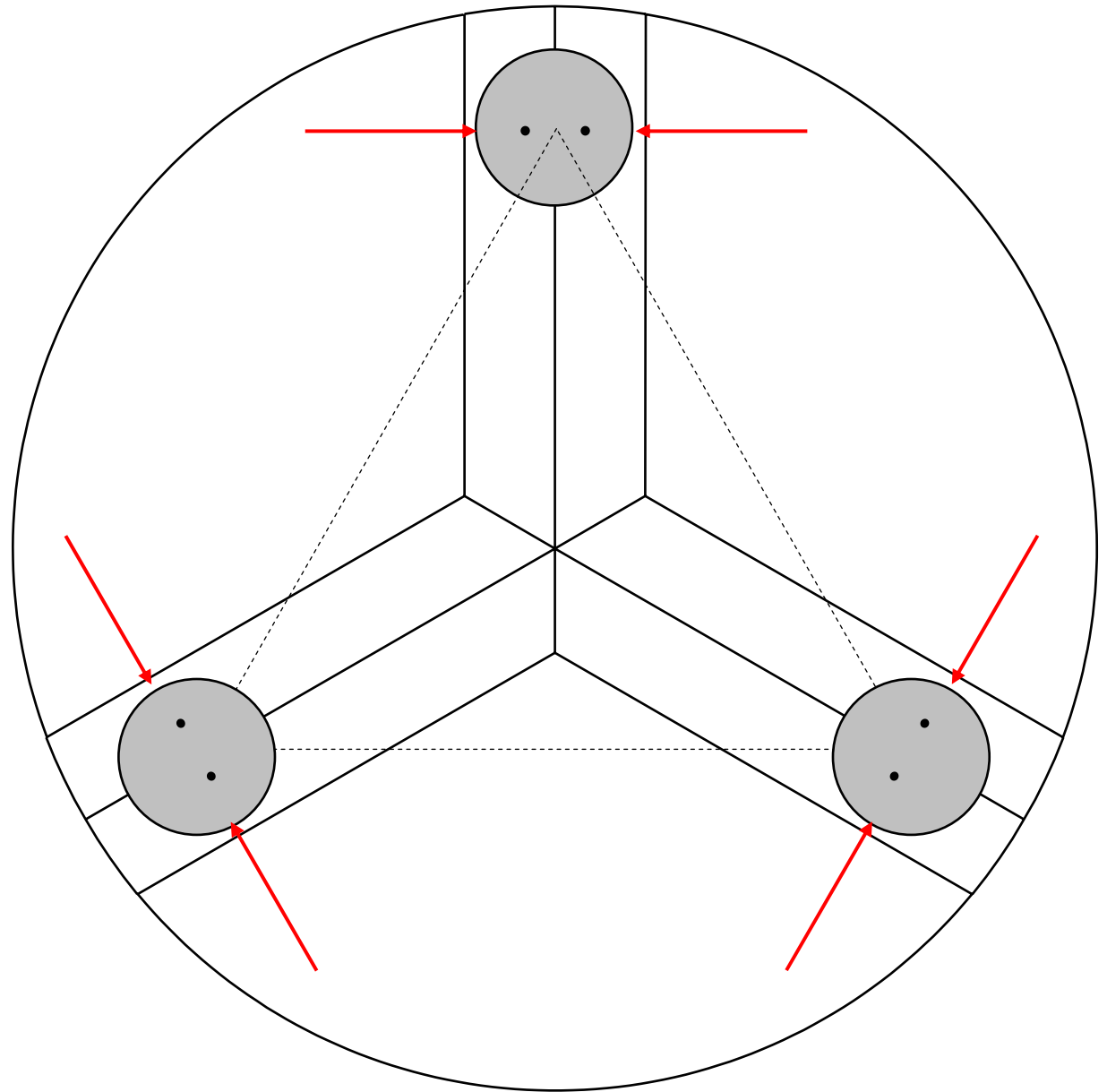
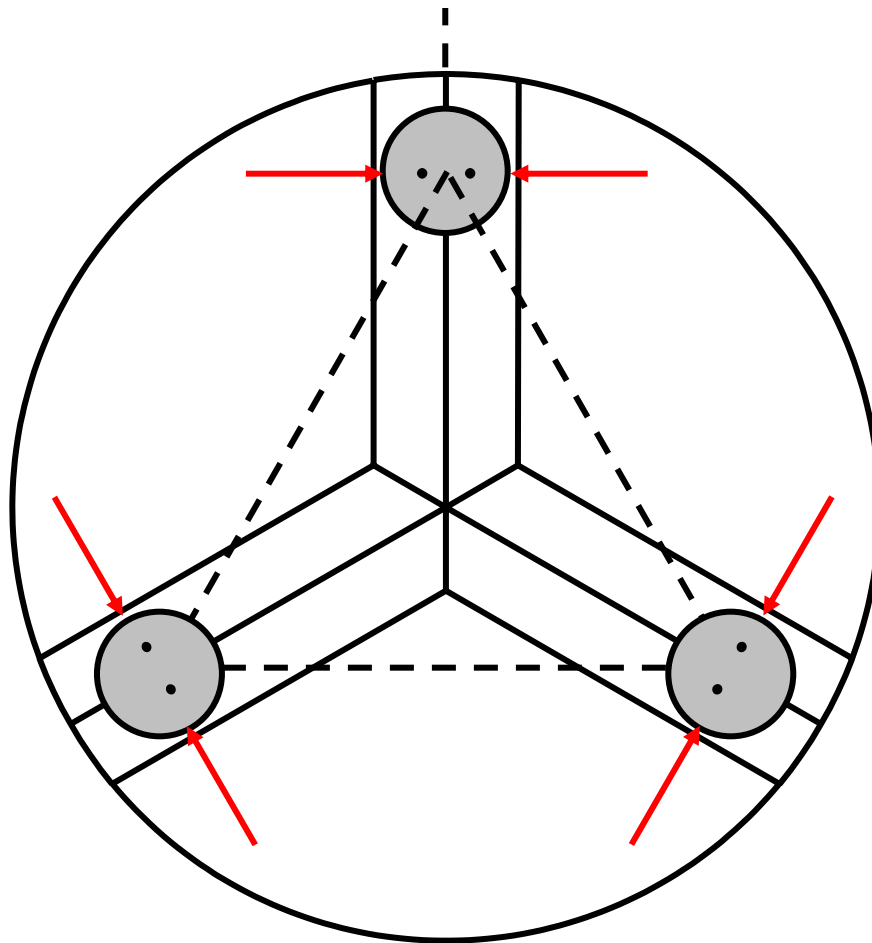
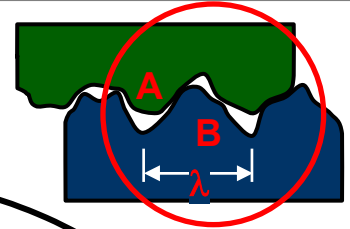


Figure: Layton Hales  
PhD Thesis, MIT.

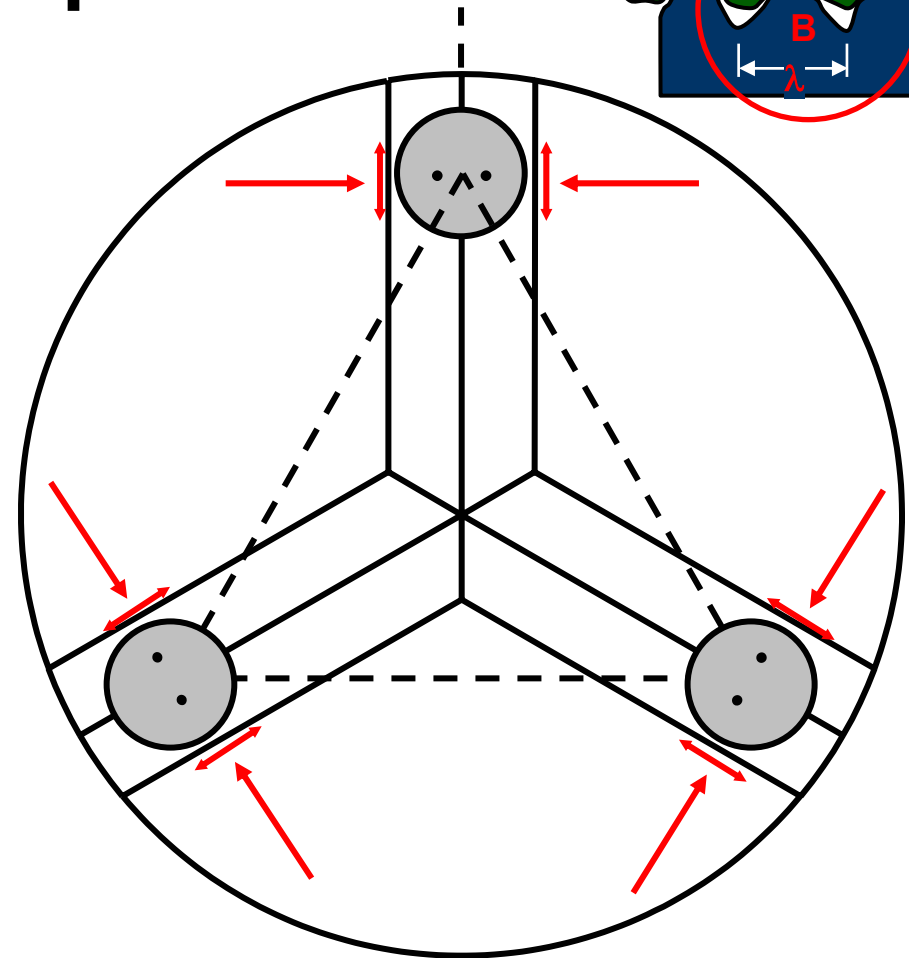


# Consequences of friction

Are kinematic couplings perfect?

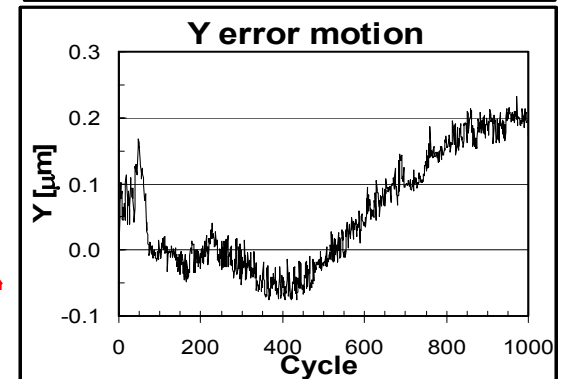
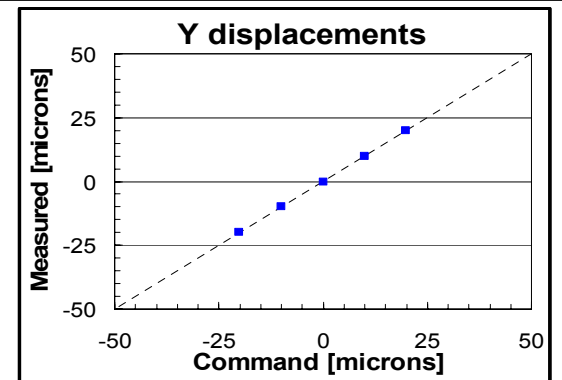
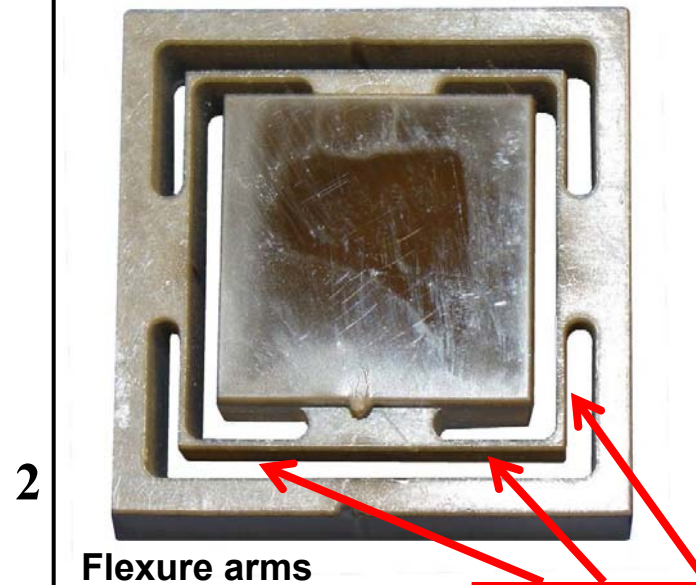
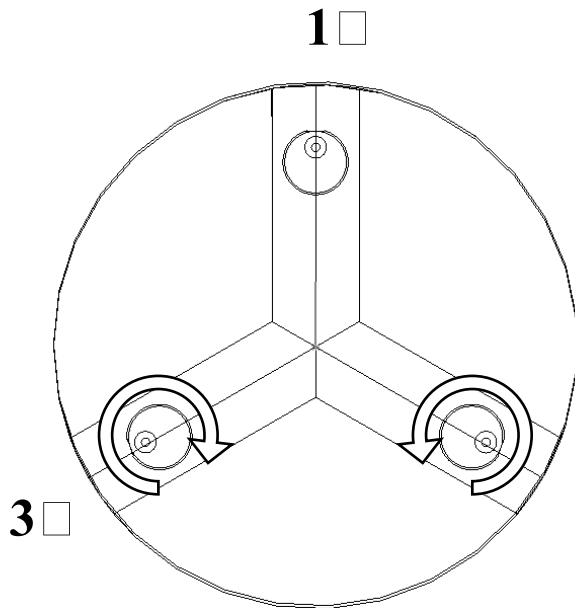


**Ideal in-plane constraints**

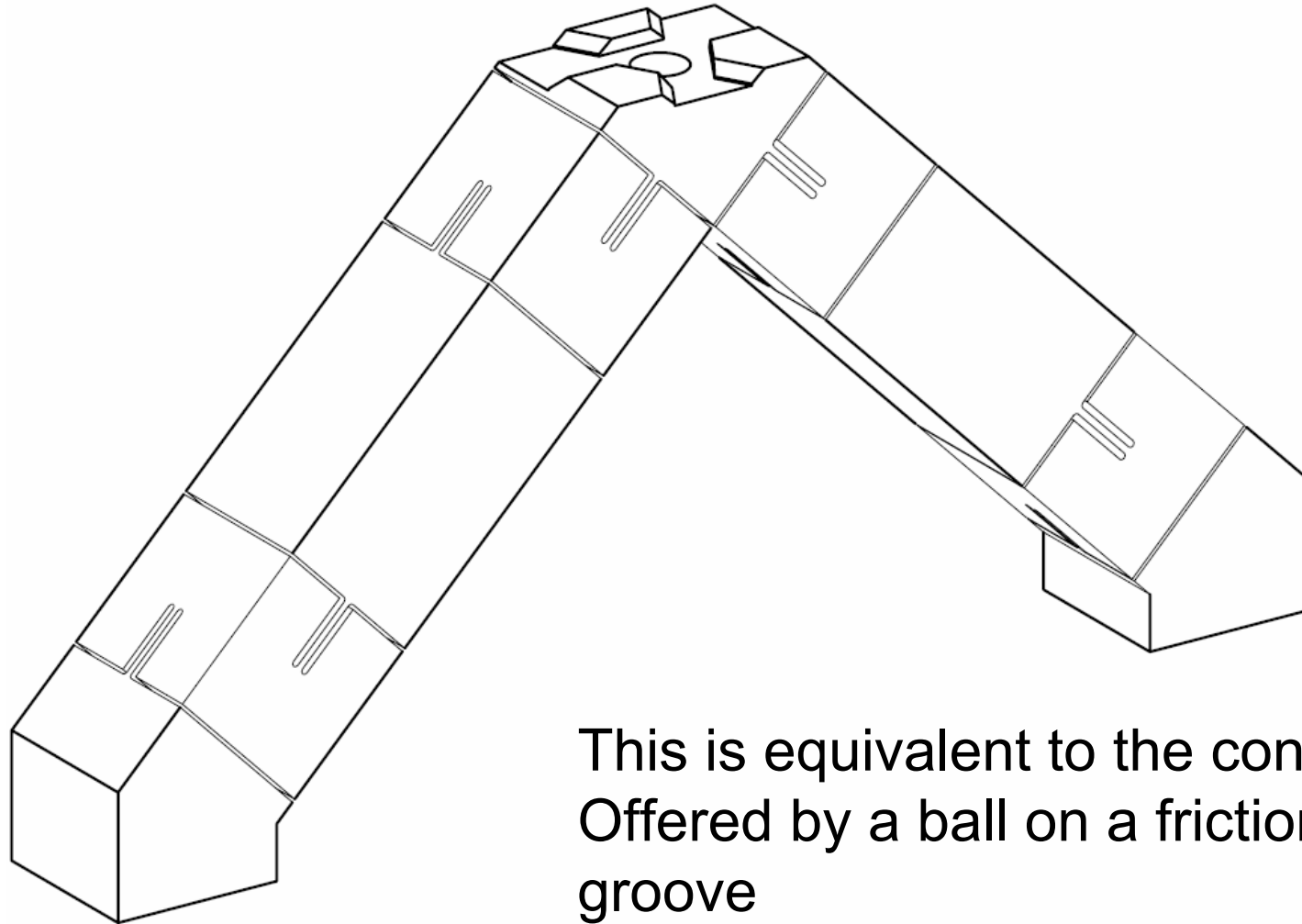


**Real in-plane constraints**

# Flexure grooves reduce friction effect



# Orrr....



This is equivalent to the constraint  
Offered by a ball on a frictionless  
groove

# Instant center visualization example

Instant center can help you identify how to best constrain or free up a mechanism

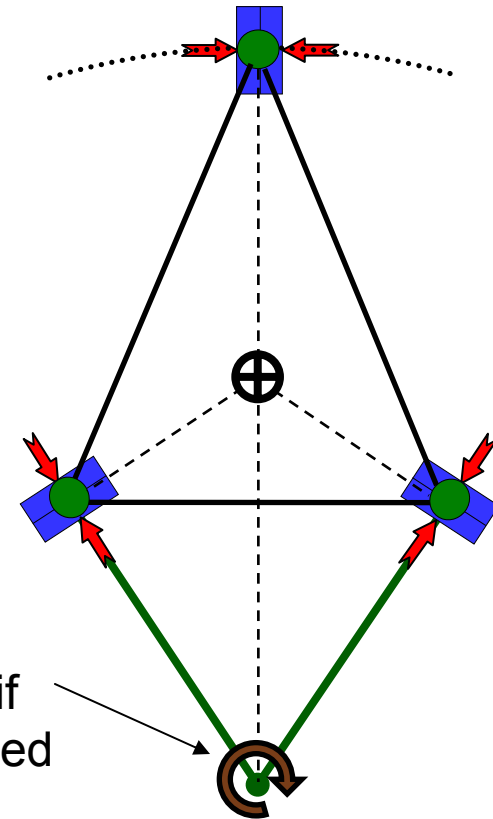
$$\frac{K_{\parallel}}{K_{\perp}} \cdot \frac{\delta_{\perp}}{\delta_{\parallel}} \rightarrow CM_k \cdot CM_{\delta} \ll 1$$

Diagram removed for copyright reasons.  
Source: Alex Slocum, *Precision Machine Design*.

Poor

Good

Instant center if  
ball 1 is removed



# Examples

Is it a wise idea to put three balls in three cones while the balls are rigidly attached to a rigid part?

$$\frac{K_{\parallel}}{K_{\perp}} \cdot \frac{\delta_{\perp}}{\delta_{\parallel}} \rightarrow CM_k \cdot CM_{\delta} \ll 1$$

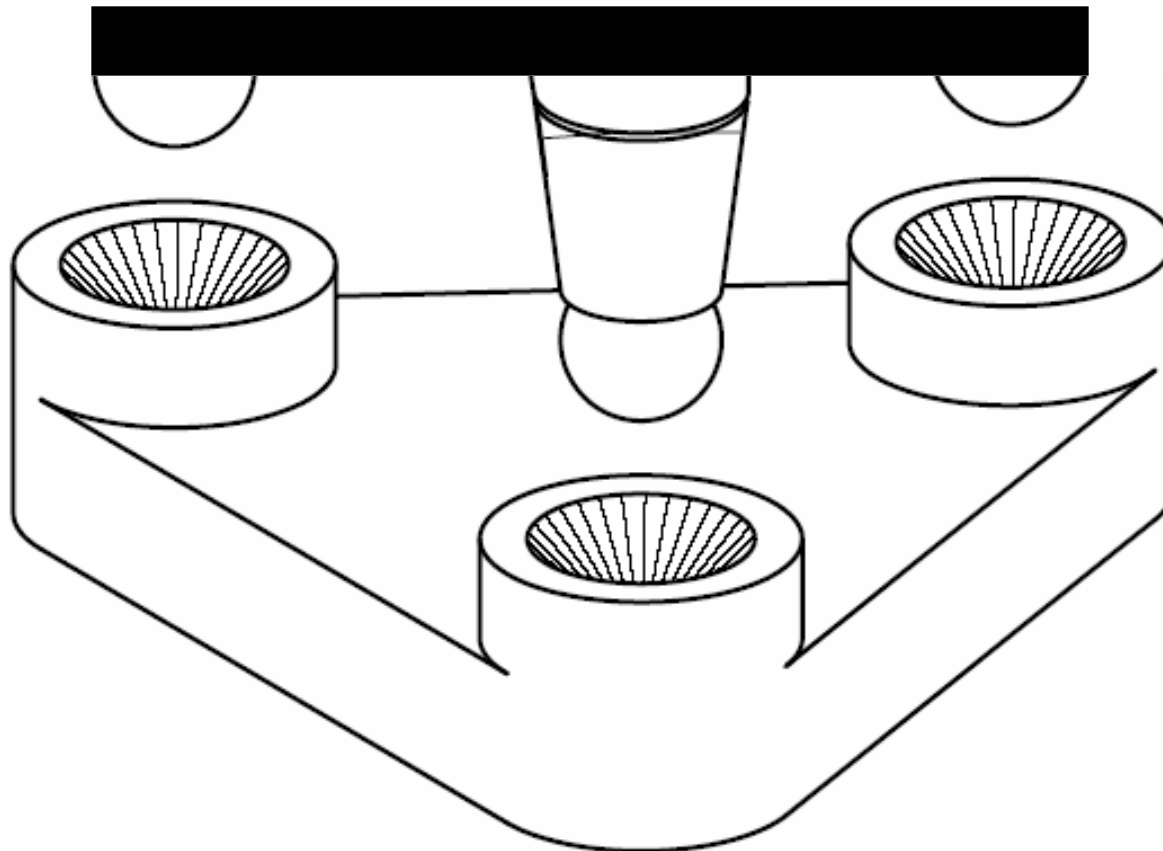
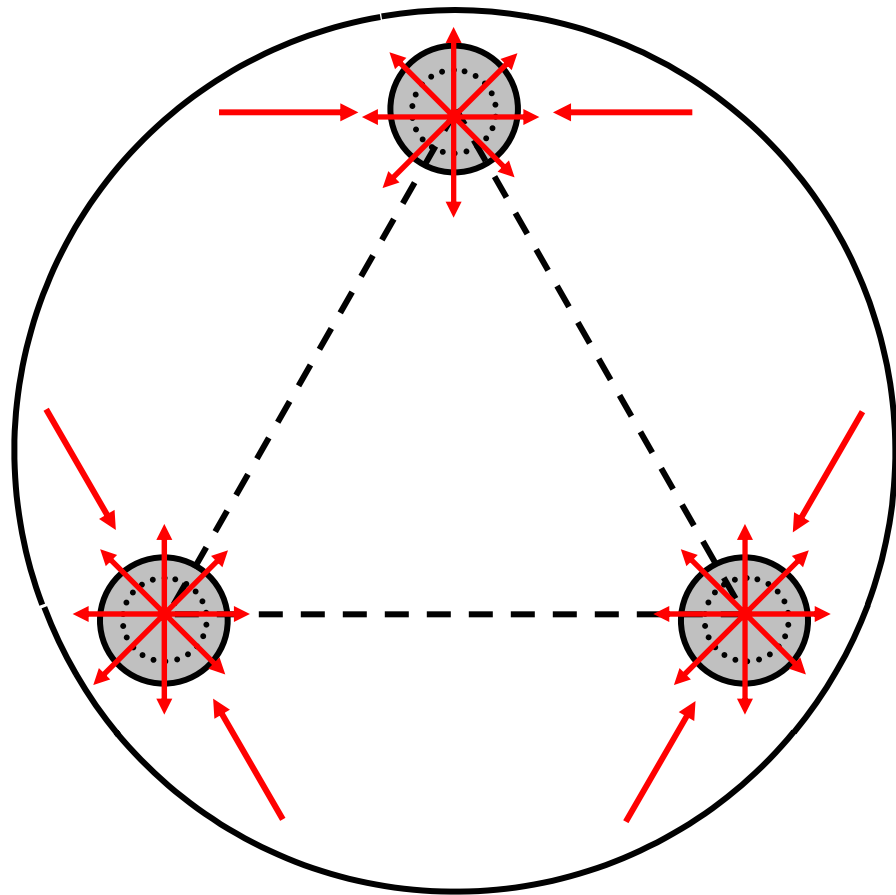
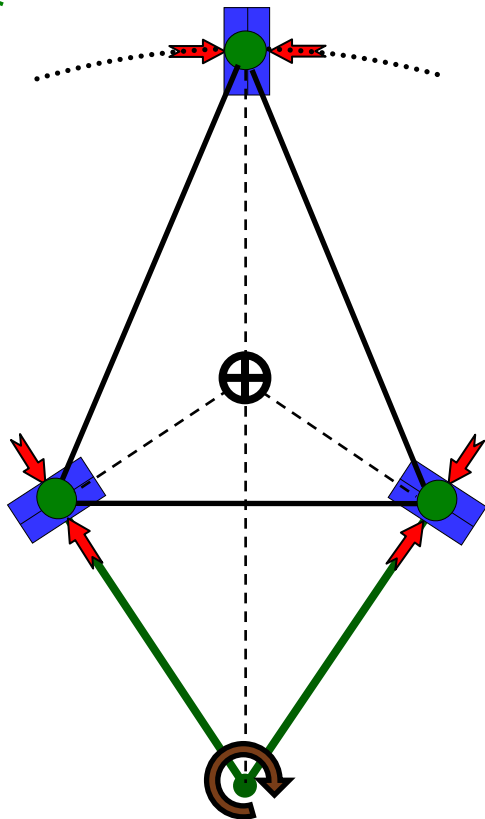
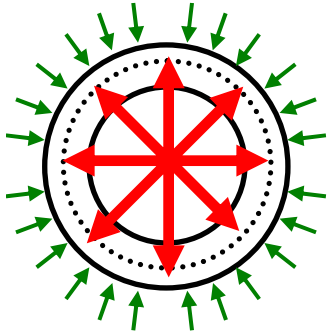


Figure: Layton Hales PhD Thesis, MIT.

# In-plane use of flexures

Three balls in three cones

What does the constraint diagram look like?





# Use of flexures to avoid over constraint

## Flexures provide a very low CM for each joint

- ❑ Energy stored due to over constraint is minimized
- ❑ Energy is channeled through continuously variable
- ❑ Is possible to reach a true minimum

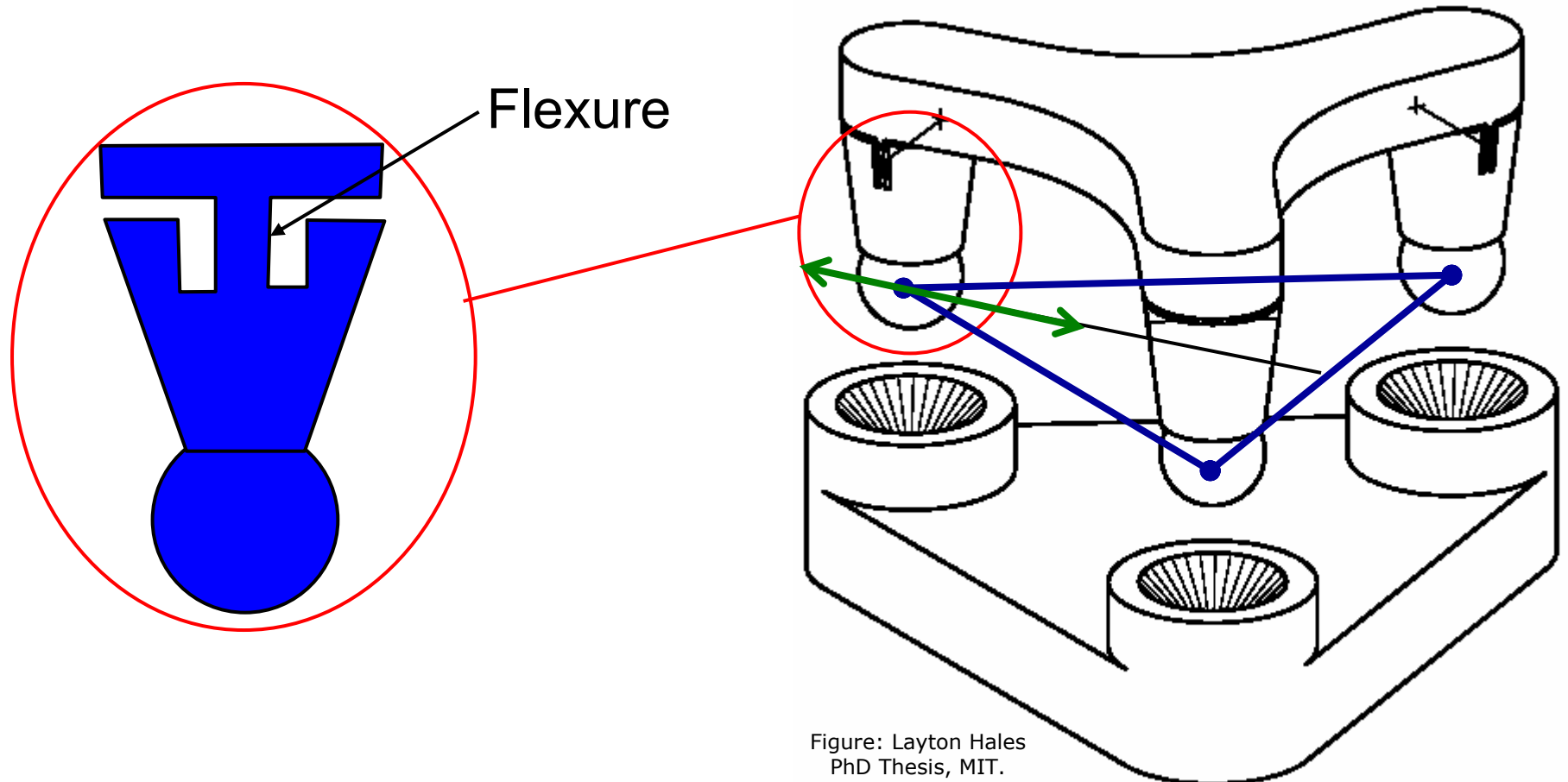
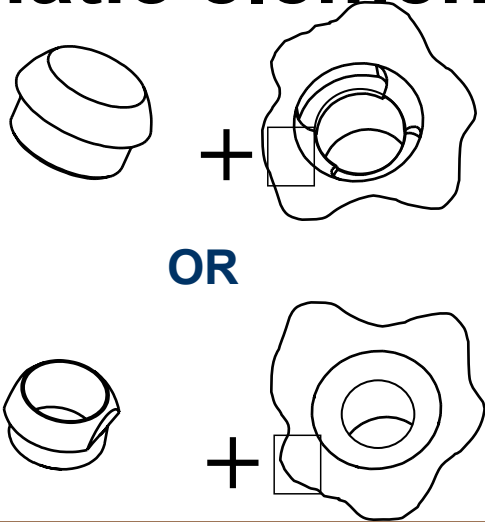


Figure: Layton Hales  
PhD Thesis, MIT.

# Low-cost couplings

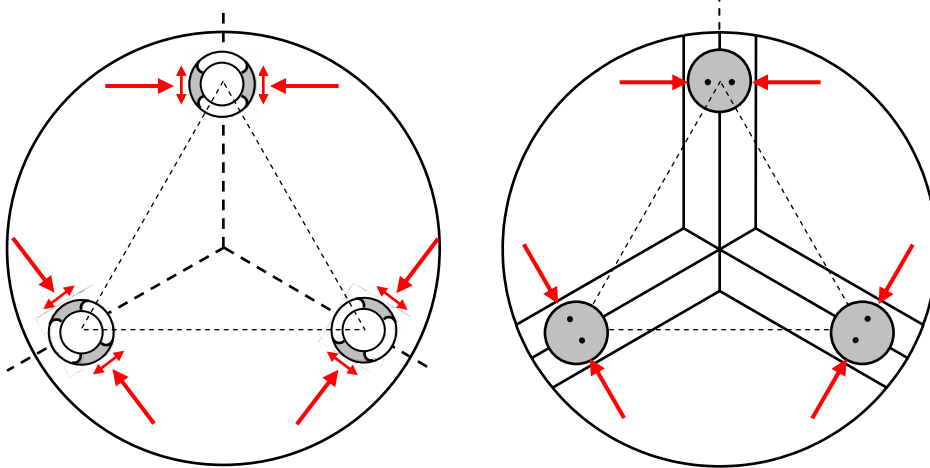
## Kinematic elements



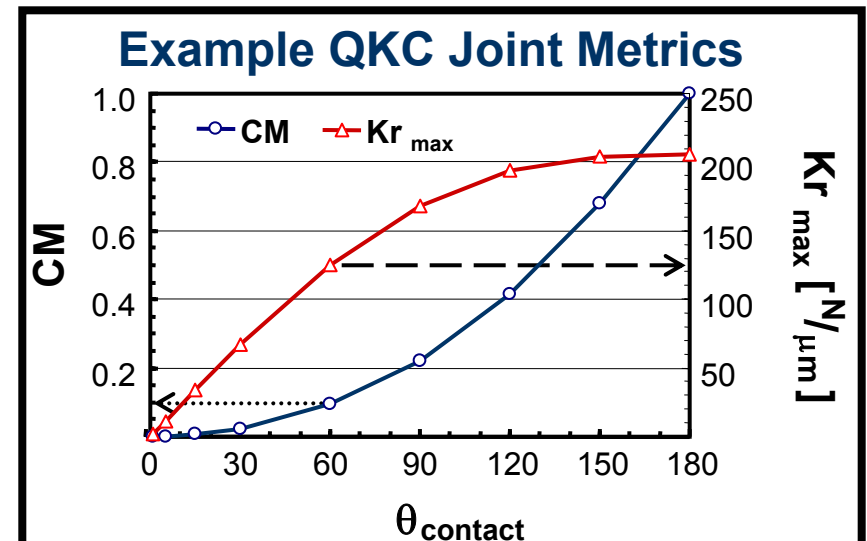
## Manufacturing

Diagrams removed for copyright reasons.  
"Cast + Form Tool = Finished"

## Constraint diagrams



## Metrics

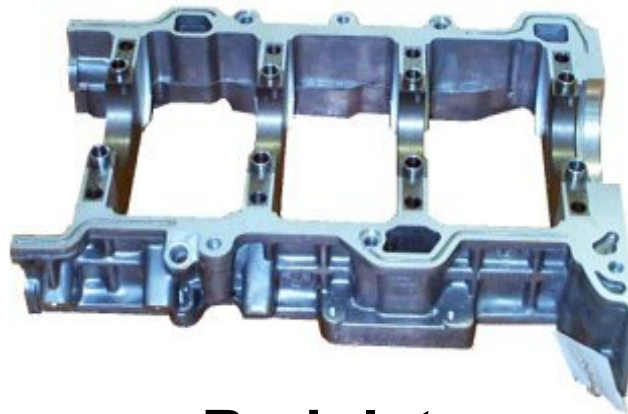


# Case study: Duratec engine

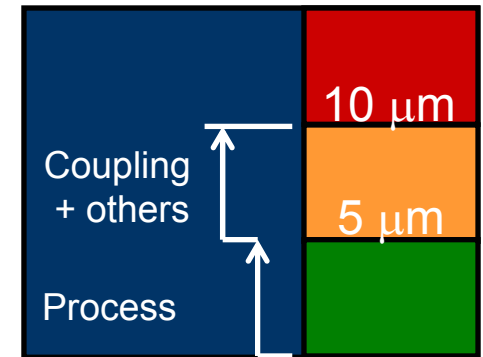
## Components



**Block**

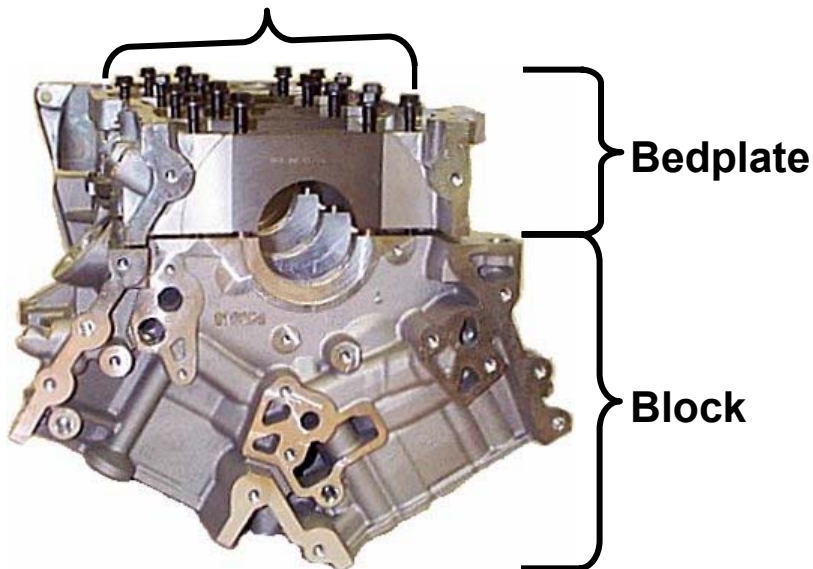


**Bedplate**

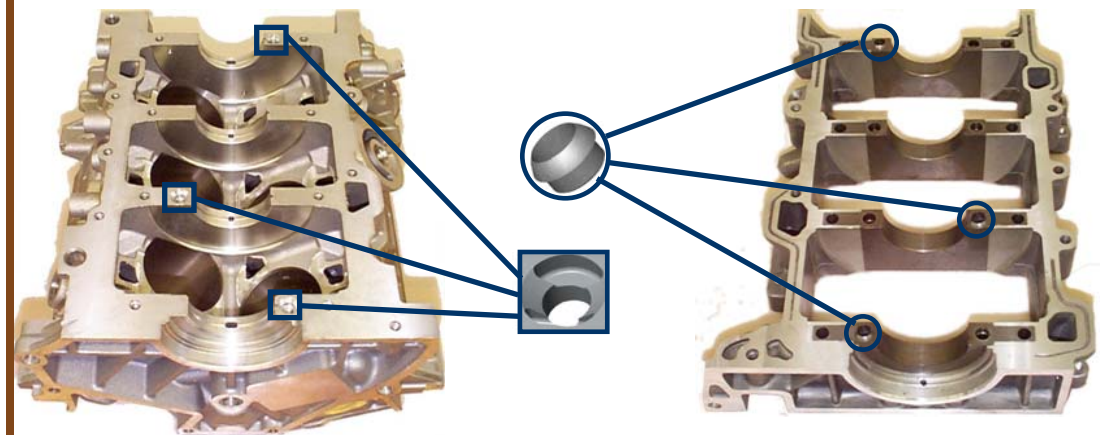


## Pinned joint

Assembly Bolts



## QKC

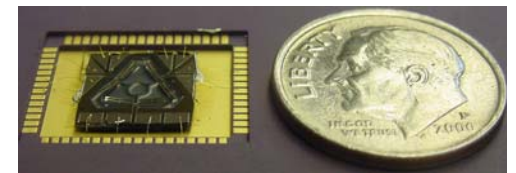
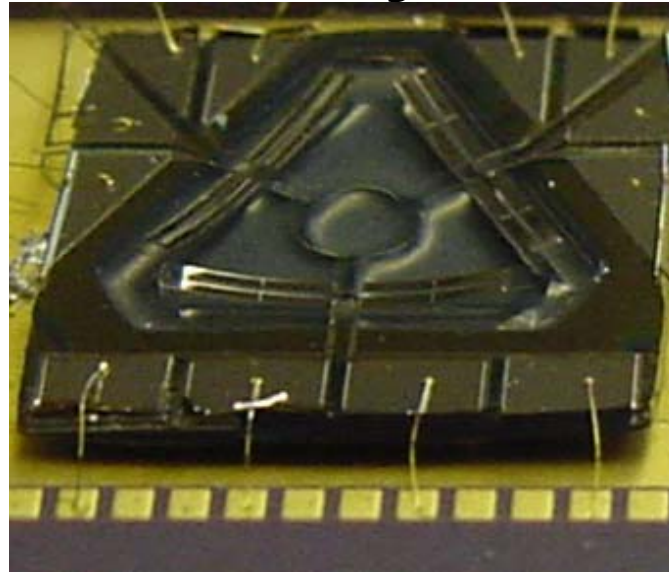


# Micro-scale systems

# Micro-scale MuSS main challenges

## Fabrication is fundamentally different

- Chemical
- Molecular
- Ballistic
  
- Finished geometry
- Possible geometries

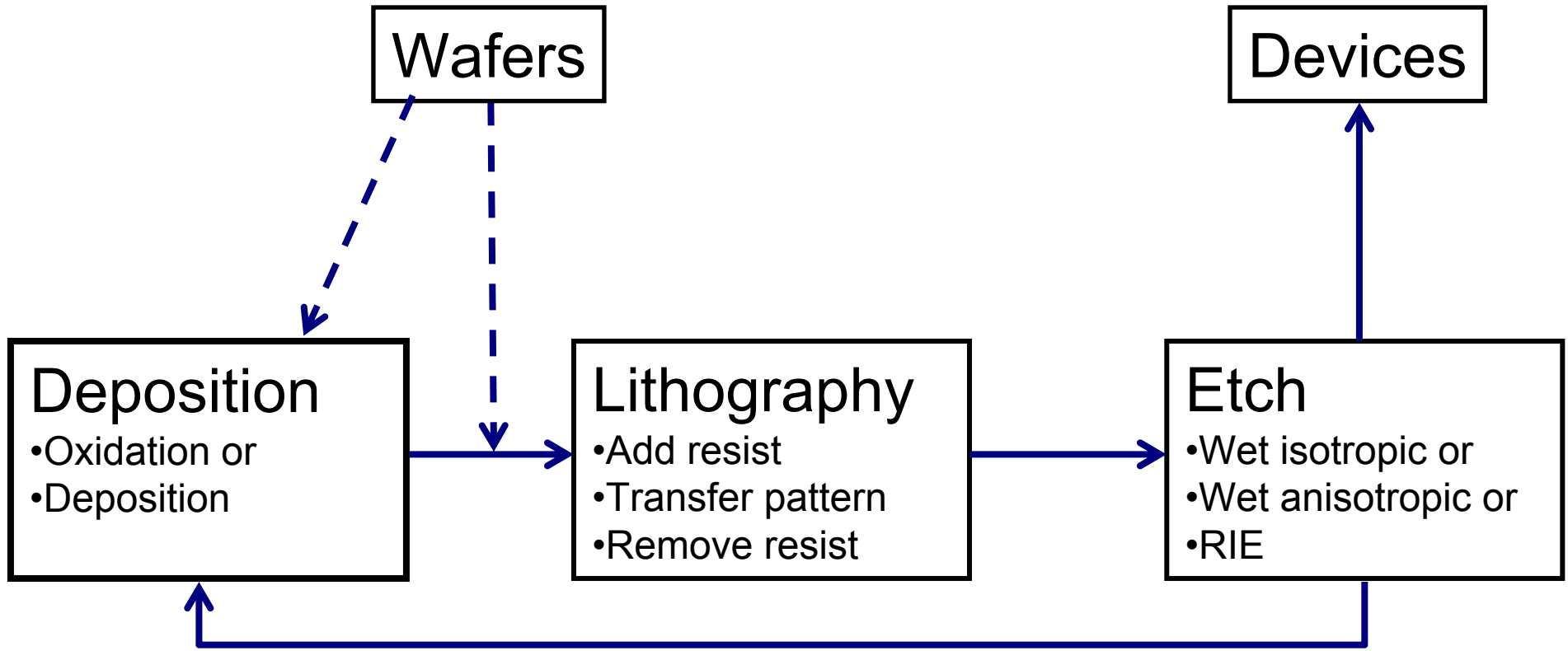


## Physics “rounding” is no longer acceptable

- Surface forces
- Thermal time constants
- Strains

# Micro-fabrication video

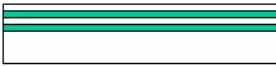





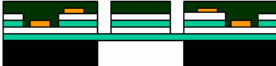


# General process



**Bulk micromachining = Removal of the wafer**

**Surface micromachining = Add/remove layers**

# MiHx fabrication

| Step  | Recipe/Description  |
|---|---|
|    | Double deck SOI; Device layers @ 8 microns thickness; Oxide at 1 micron thickness |
|    | Photoresist and pattern   |
|    | DRIE (Si) and BOE Oxide   |
|    | Pattern AL contacts at 350 nm thickness   |
|    | Photoresist and pattern   |
|   | DRIE (Si) and BOE Oxide and DRIE (Si)   |
|  | Pattern handle wafer; Mount to quartz wafer; DRIE backside etch                   |
|  | Release with vapor HF   |
|  | Remove resist via plasma etch   |





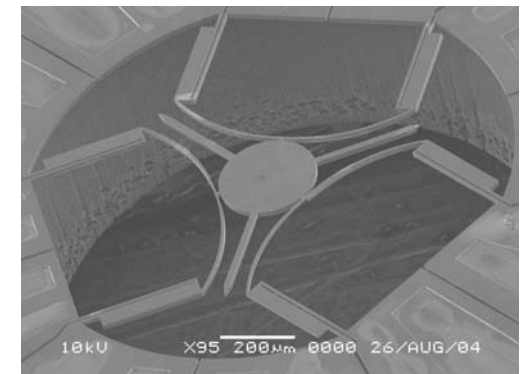
# Micro-scale physics

**For strong dependence on characteristic length, importance of phenomena decreases with characteristic dimension**

- Gravity  $L^3$
- Inertia  $L^3$

**For weaker dependence on characteristic length, phenomena become dominate at small scale**

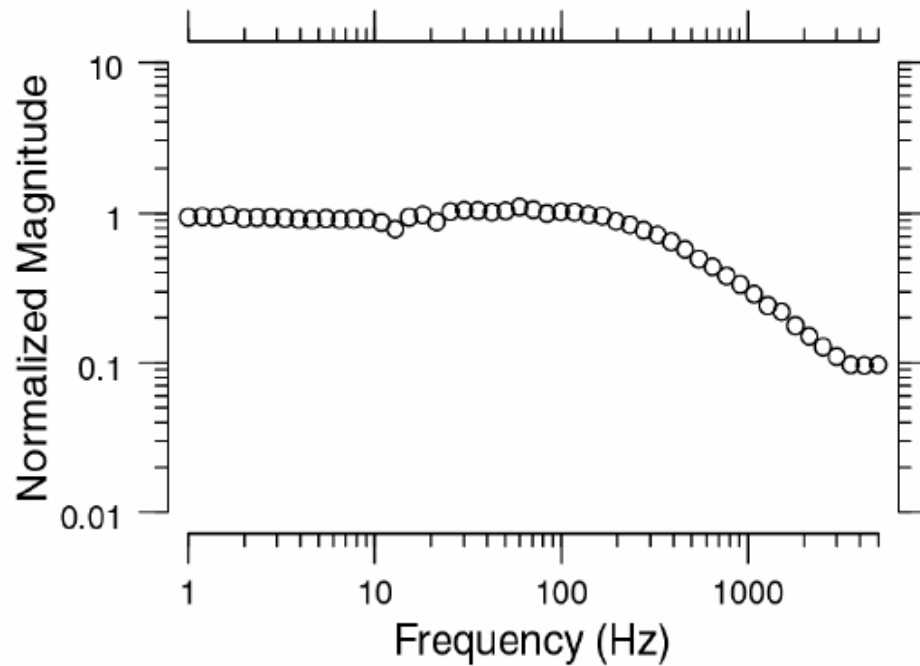
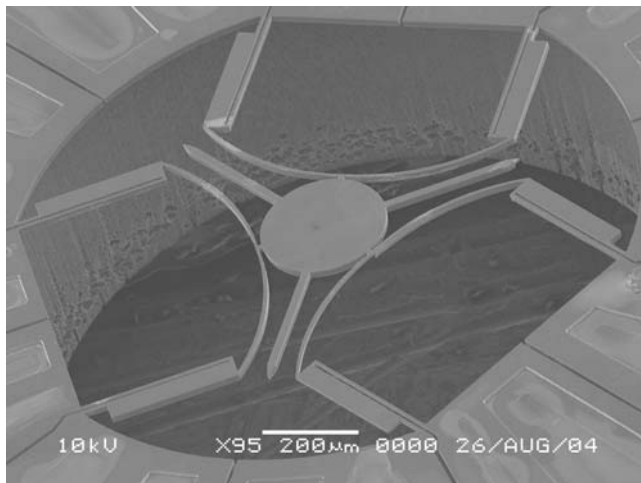
- Electrostatic  $L^2$
- Surface tension  $L^2$
- Thermal  $L$



# Thermal physics

Ratio of surface area to volume increases

Where does this help?



Where does this hurt?

# Assignment

**Design a mechanical filter system (may be more than one flexure which is capable of reducing actuator input by a factor of 100. The reduction is called the transmission ratio = output/input**

## Design constraints

- 5 x 5 envelope
- 1/4 inch thick
- Flexures should be movable by hand
- Stress less than 20% of yield stress
- Actuator range = 0 – 150 microns
- Actuator resolution = 10 nanometers