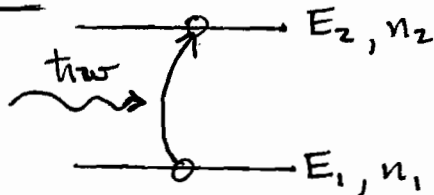


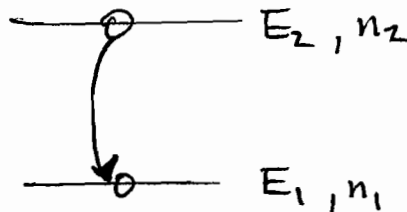
SPONTANEOUS VS. STIMULATED EMISSION

- 2 LVL. SYS.

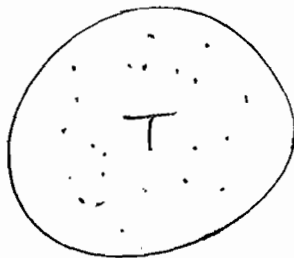
ABSORPTION

$$E_n = - \frac{13.6 \text{ eV}}{n^2}$$

$$h\nu = E_2 - E_1$$

EMISSIONSPONTANEOUS  
EMISSION

THINK ABOUT MOLECULES IN A BLACKBODY CONTAINER (IN A RADIATION FIELD)  
AT THERMAL EQUILIBRIUM AT TEMP.,  $T$ .



FOR A 2-LVL.-SYS., THE RELATIONSHIP BETWEEN  $n_2$  &  $n_1$  IS

$$\frac{n_2}{n_1} = \exp\left(\frac{-E_2 - E_1}{kT}\right)$$

$\uparrow$   $1.38 \times 10^{-23} \text{ J/K}$

ABSORPTION -

$$-\frac{dn_1}{dt} = B_{12} n_1 u(\nu, T)$$

$$\uparrow \text{PLANCK'S LAW} = \frac{8\pi h\nu^3}{c^3} \cdot \frac{1}{e^{h\nu/kT} - 1}$$

CANNOT  
EQUATE  
ALONE

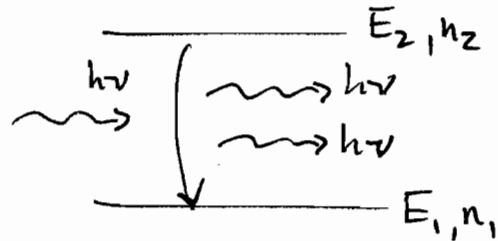
SPONTANEOUS EMISSION -

$$-\frac{dn_2}{dt} = A_{21} n_2$$

∴ ALSO NEED,

STIMULATED EMISSION -

$$-\frac{dn_2}{dt} = B_{21} n_2 u(\nu, T)$$

STIMULATED  
EMISSION

$$\sum \frac{dn_i}{dt} = 0 \Rightarrow$$

$$B_{12} n_1 u(\nu, T) = B_{21} n_2 u + A_{21} n_2$$

$$B_{12} = B_{21}$$

$$A_{21} = \frac{8\pi h\nu^3}{c^3} B_{12}$$

IN A RADIATION FIELD, STIMULATED EMISSION EXISTS

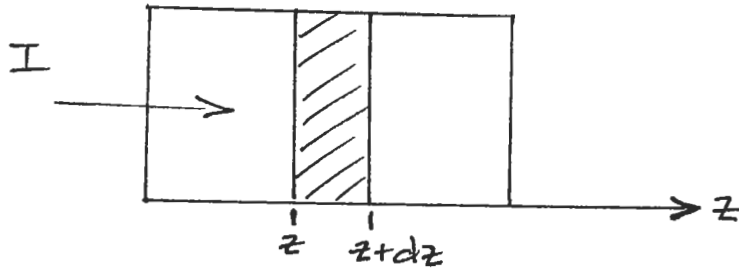
eg., EXAMINE THERMAL RADIATION

$$\text{LET } m = \frac{\text{STIMULATED}}{\text{SPONTANEOUS}} = \frac{1}{e^{h\nu/kT} - 1}$$

$$kT \approx 26 \text{ meV @ } 300\text{K}$$

$$1 \mu\text{m} \rightarrow h\nu \approx 1.24 \text{ eV}$$

∴ AT RT STIMULATED EMISSION IS NOT VERY APPARENT



$$I = cu \quad (4\pi \text{ SPONTANEOUS})$$

$$dI = -h\nu B_{12} n_1 u dz + h\nu B_{21} u dz$$

$$dI = -\alpha I dz$$

$$\alpha = \frac{h\nu}{c} B_{12} \left( \frac{g_2}{g_1} n_1 - n_2 \right)$$

NOTE: AT EQUIL.  $n_1 > n_2$

$$\therefore \alpha > 0$$

$$I = I(0) e^{-\alpha z}$$

IF  $\alpha$  IS NEGATIVE, i.e.  $n_2 > n_1$  (POPULATION INVERSION)

$$-\alpha = \gamma \equiv \text{gain (AMPLIFICATION)}$$

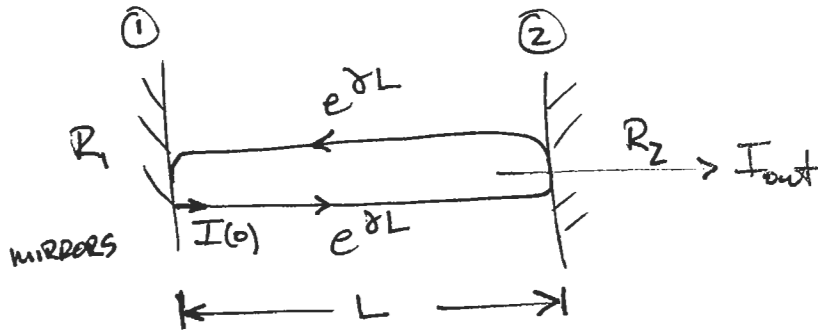
\* SOME PEOPLE CALL POP. INV. A (-)VE TEMP PROCESS, BASED ON  $\frac{n_2}{n_1} > 1 \Rightarrow \exp\left(\frac{E_1 - E_2}{kT}\right) > 1$  WHICH IMPLIES (-)VE TEMP. BUT FOR POP. INV. THE PROCESS IS NON-EQUIL. AND  $\frac{n_2}{n_1} = \exp\left(\frac{-E_2 - E_1}{kT}\right)$  DOES NOT APPLY

POP. INV.

$$\frac{g_2}{g_1} n_1 - n_2 < 0$$

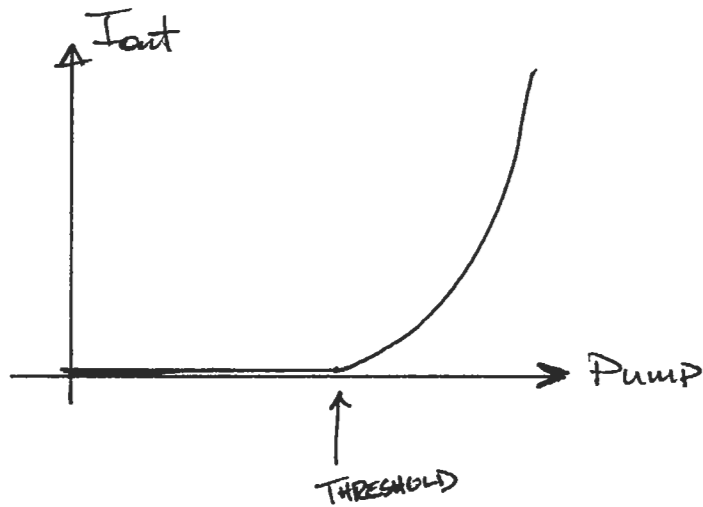
$g \equiv \text{DEGENERACY}$

## MIRROR CAVITY



$$I(0) R_1 R_2 e^{2\delta L} e^{-2\beta L} = I(0)$$

$$\gamma = \beta - \frac{1}{2L} \ln(R_1 R_2)$$

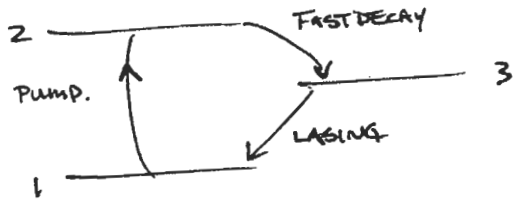
TYPICAL CURVEPUMPING

WANT  $n_2 > n_1$

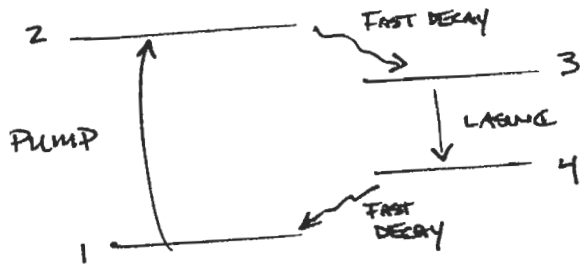
... SOLVING SPONTANEOUS EMISSION EQN.

$$n_2 = n_2(0) e^{-t/\tau_{span}} \quad ; \quad \tau_{span} = \frac{1}{A_{21}}$$

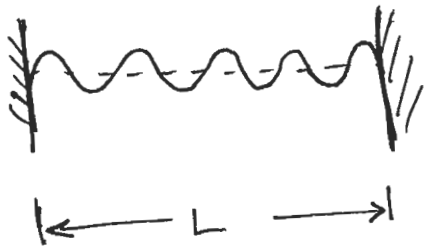
3-LVL-SYS.



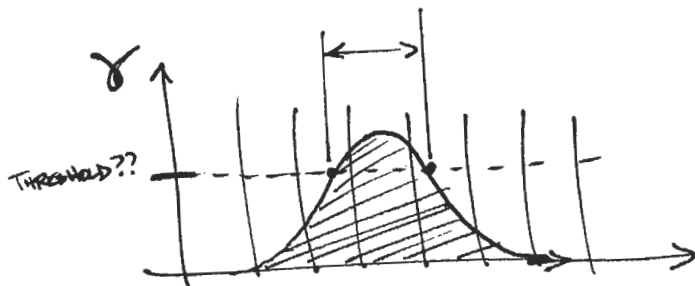
4-LVL-SYS.



LASER BEAM CHARACTERISTICS



↑ INTEGER  
 $\frac{\lambda}{2} \cdot n = L$



LONGITUDINAL MODES

SPACING  $\Delta\nu = \frac{c}{\lambda} = \frac{2nc}{L}$

$c \sim 10^8 \text{ m/s}$

$\gamma_0 \sim 10^{14}$

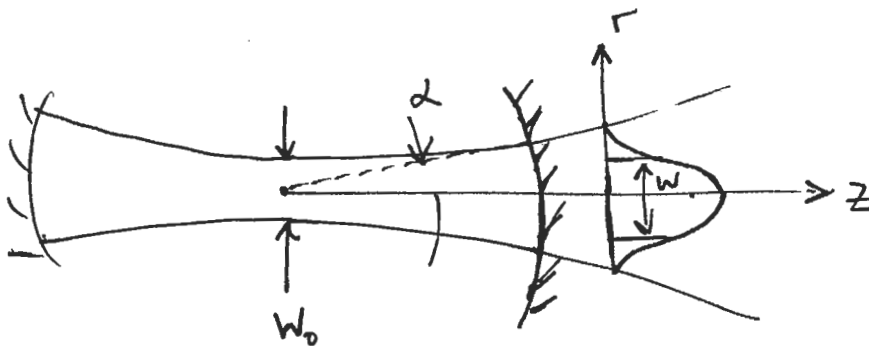
... COULD ALSO HAVE TRANSVERSE WAVES



A CAVITY w/ CURVED MIRRORS -



$$0 \leq \left(1 - \frac{L}{r_1}\right) \left(1 - \frac{L}{r_2}\right) \leq 1$$



GAUSSIAN BEAM OPTICS

$$I(r, z) = I_0 e^{-2r^2/w^2(z)}$$

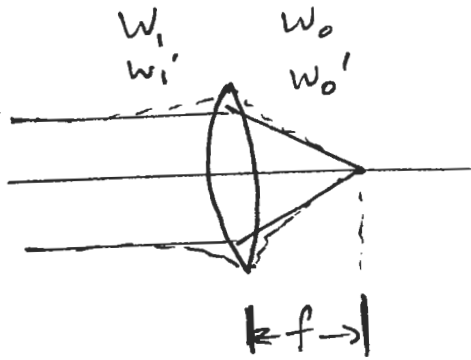
$$w(z) = w_0 \left[ 1 + \left( \frac{z}{z_0} \right)^2 \right]^{1/2}$$

$$\alpha = \frac{\lambda}{\pi w_0}$$

$$z_0 = \frac{\pi w_0^2}{\lambda}$$

$$w_0 = \left( \frac{\lambda L}{\pi} \right)^{1/2} \left[ \frac{(r_1 - L)(r_2 - L)(r_1 + r_2 - L)}{L(r_1 + r_2 - 2L)^2} \right]^{1/4}$$

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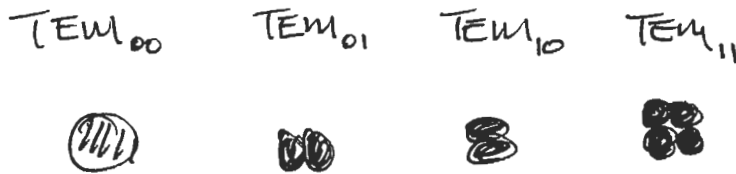


CAN USE MATRIX  
 METHOD TO COMPUTE RELATE  
 OPTICAL INPUT & OUTPUT

ABCD LAW (FROM  $\begin{pmatrix} W_o \\ W_o' \end{pmatrix} = \begin{pmatrix} A & B \\ C & D \end{pmatrix} \begin{pmatrix} W_i \\ W_i' \end{pmatrix}$ )

$$\begin{pmatrix} W_o \\ W_o' \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ -\frac{1}{f} & 0 \end{pmatrix} \begin{pmatrix} W_i \\ W_i' \end{pmatrix}$$

MODES TEM<sub>mng</sub>



TYPES OF LASERS

ACTIVE MEDIA { GAS  
 LIQUID  
 SOLID

WAVELENGTH { EXCIMER  
 VISIBLE  
 NEAR INFRARED  
 MIDDLE I.R. (CO<sub>2</sub>)

PUMP METHOD { OPTICAL  
 ELECTRICAL

S.C. LASERS.

—————  $E_c$

—————  $E_v$

