

- > Welcome to 16.90 iSession ...
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 - ...etc...
 - ...etc...

Reading recap

- Stiffness
 - Orders of magnitude difference in timescales
 - Eigenvalues determines time scale $\frac{dy}{dt} = \lambda u$
- Newton Raphson
 - Implicit schemes benefit stiff ODEs.
 - Each step requires solving a nonlinear algebraic equation
 - Newton Raphson solves such nonlinear algebraic equations

$$\frac{dy}{dt} = \lambda u$$

$$V^{n+1} = V^{n-1} + \underbrace{2\Delta t (\lambda u^n)}$$

$$\begin{cases} V^{n+1} = V^0 z^{n+1} \\ V^n = V^0 z^n \\ V^{n-1} = V^0 z^{n-1} \end{cases}$$

$$|z| = \sqrt{\operatorname{Re}(z)^2 + \operatorname{Im}(z)^2}$$

A transient thermal problem

- **An aluminum plate and a copper plate initially at room temperature.**
- **One plate Heated by hot air at time $t=t_0$.**
- **Predict the measured temperature as a function of time.**
- **Is it a stiff problem? Why or why not?**

$$\dot{Q}_{\text{cond}} = k A \frac{\Delta T}{\Delta x}$$

$$\Delta T = T_A - T_c$$

$$m_A c_A \frac{\partial T_A}{\partial t} = \dot{Q}_{\text{conv}} - \dot{Q}_{\text{cond}}$$

$$A \left(\frac{\partial T_A}{\partial t} \right) = \left(\frac{kA}{m_A c_A \Delta x} \right) (T_A - T_c) + \frac{hA(T_{\text{air}} - T_A)}{m_A c_A}$$

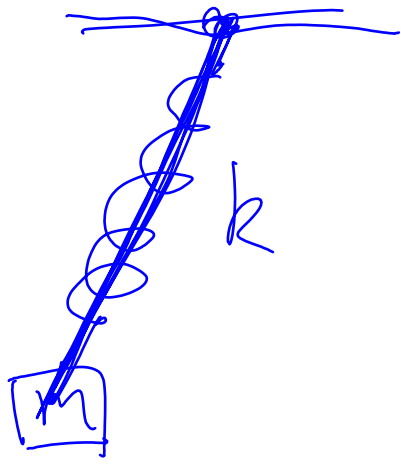
$$\frac{\partial T_c}{\partial t} = \frac{kA}{m_c c_c} \frac{T_A - T_c}{\Delta x} - \frac{hA(T_c - T_{\text{air}})}{m_c c_c}$$

$$\frac{\partial}{\partial t} \begin{pmatrix} T_A \\ T_C \end{pmatrix} = \begin{pmatrix} -L - s & +L \\ L & -L - s \end{pmatrix} \begin{pmatrix} T_A \\ T_C \end{pmatrix}$$

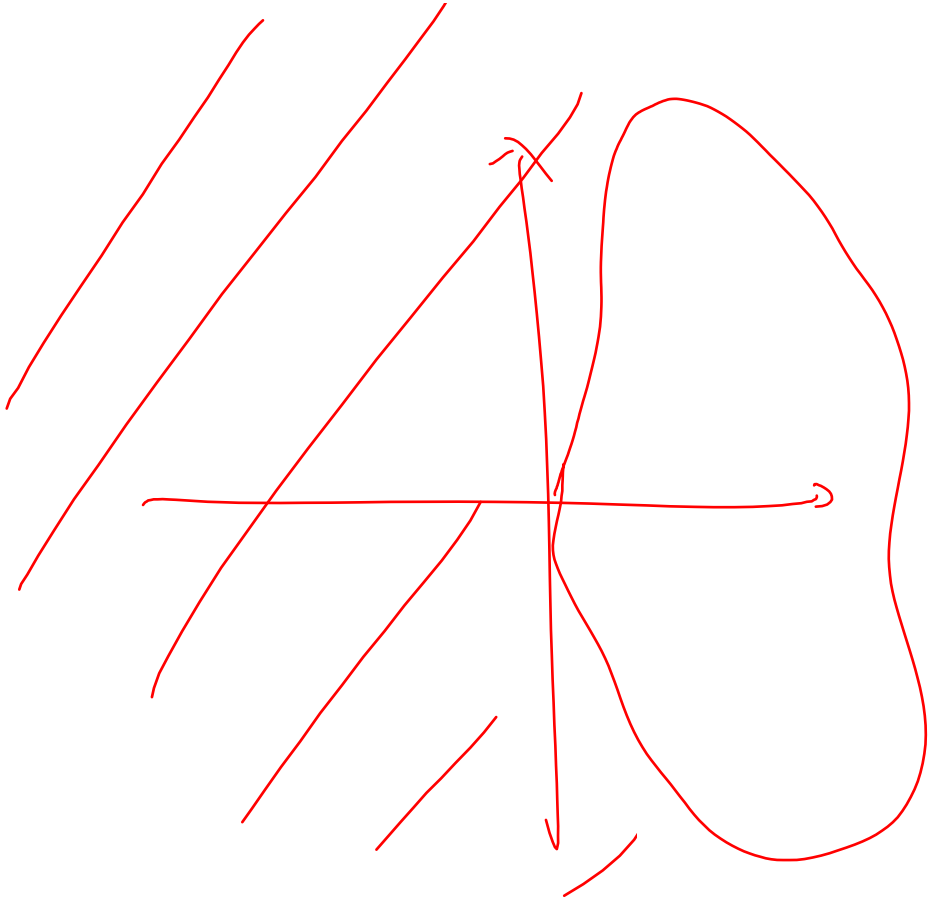
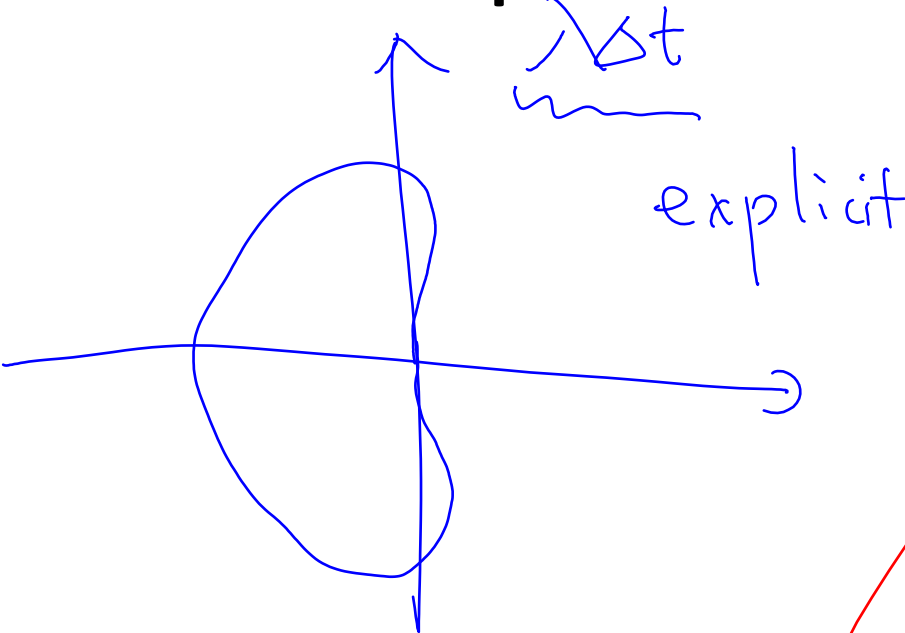
$$\text{eig} \begin{pmatrix} -L & L \\ L & -L \end{pmatrix}$$

$$L \cdot \text{eig} \begin{pmatrix} -1 & 1 \\ 1 & -1 \end{pmatrix} = \underbrace{0}_{\text{slow}}, \underbrace{-2L}_{\text{fast}}$$

$$\text{eig} \begin{pmatrix} -L - s & L \\ L & -L - s \end{pmatrix} = \underbrace{-s}_{\text{slow}}, \underbrace{+2L - s}_{\text{fast}}$$



Newton Raphson for implicit scheme



$$\frac{V^{n+1} - V^n}{\Delta t} = f(V^{n+1})$$

Linear: $f(V^{n+1}) = AV^{n+1}$

$$\left(\frac{I}{\Delta t} - A\right)V^{n+1} = \frac{V^n}{\Delta t}$$

$$\Delta V = V^{n+1} - V^n$$

Nonlinear
It #1

$$f(V^{n+1}) \approx \underbrace{f(V^n)}_{\text{known}} + \underbrace{\left(\frac{\partial f}{\partial V} \Big|_{V^n}\right)}_{\text{known}} \cdot \underbrace{\Delta V}_{\text{unknown}}$$

$$\frac{\Delta V}{\Delta t} = f(v^n) + \left(\frac{\partial f}{\partial v} \Big|_{v^n} \right) \Delta V$$

$$\left(\frac{1}{\Delta t} - \left(\frac{\partial f}{\partial v} \right) \right) \Delta V = f(v^n)$$

$$\underbrace{v^{n+1}} = v^n + \Delta V$$

$$\frac{\underbrace{v^{n+1}} - v^n}{\Delta t} \Rightarrow f(\underbrace{v^{n+1}}) \quad \text{if not good enough}$$

$$v^{n+1} = \underbrace{v^{n+1}} + \Delta V \leftarrow \text{new } \partial v$$

It # 2

$$f(V^{n+1}) = f(\tilde{V}^{n+1}) + \left(\frac{\partial f}{\partial V} \Big|_{\tilde{V}^{n+1}} \right) \cdot \Delta V$$

$$\frac{\tilde{V}^{n+1} - V^n + \Delta V}{\Delta t} = f(\tilde{V}^{n+1}) + \left(\frac{\partial f}{\partial V} \Big|_{\tilde{V}^{n+1}} \right) \Delta V$$

$$\left(\frac{1}{\Delta t} - \left(\frac{\partial f}{\partial V} \right) \right) \Delta V = \underbrace{f(\tilde{V}^{n+1}) - \frac{\tilde{V}^{n+1} - V^n}{\Delta t}}$$

$$\tilde{V}^{n+1} = V^{n+1} + \Delta V$$

$$\underline{A} \cdot \Delta V = R \quad \Delta V = \underline{A}^{-1} R$$

$$\Delta V = \begin{pmatrix} V_1 \\ V_2 \\ \vdots \\ V_n \end{pmatrix}$$

$$R = \begin{pmatrix} R_1 \\ \vdots \\ R_n \end{pmatrix}$$

$$A = \begin{pmatrix} \frac{\partial R_1}{\partial V_1} & \dots & \frac{\partial R_1}{\partial V_n} \\ \vdots & & \vdots \\ \frac{\partial R_n}{\partial V_1} & \dots & \frac{\partial R_n}{\partial V_n} \end{pmatrix}$$

$$\Delta V = \underbrace{A^{-1}} R$$

$$\begin{array}{c} A \backslash R \\ \equiv A^{-1} R \end{array}$$

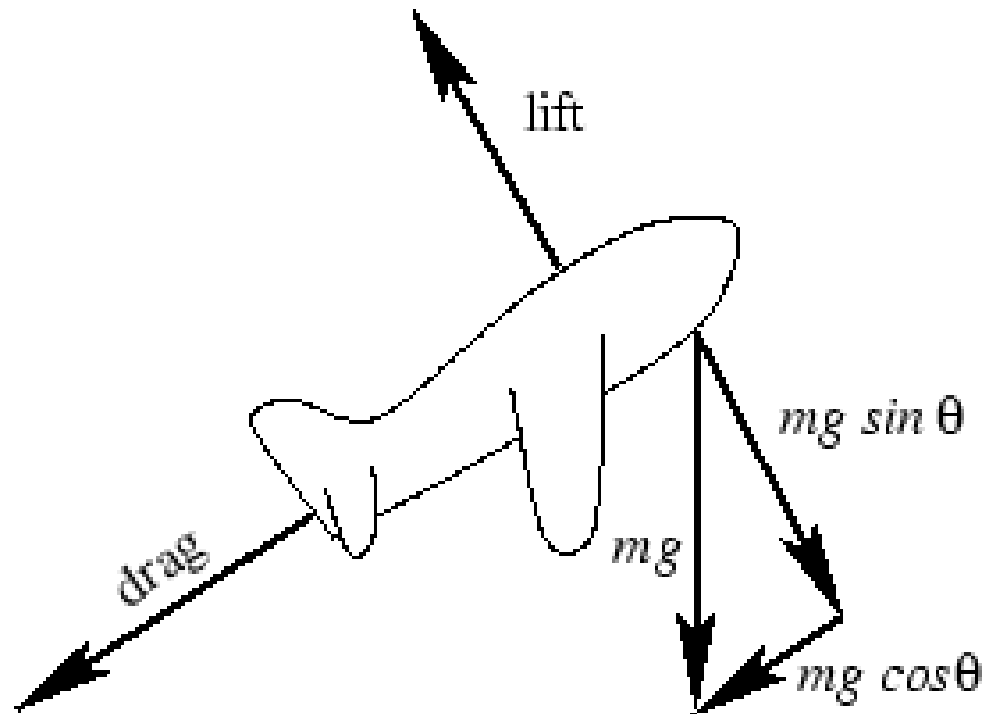
A real example of stiff system



Courtesy of [dancili](#) on Flickr. CC license BY-NC-SA.

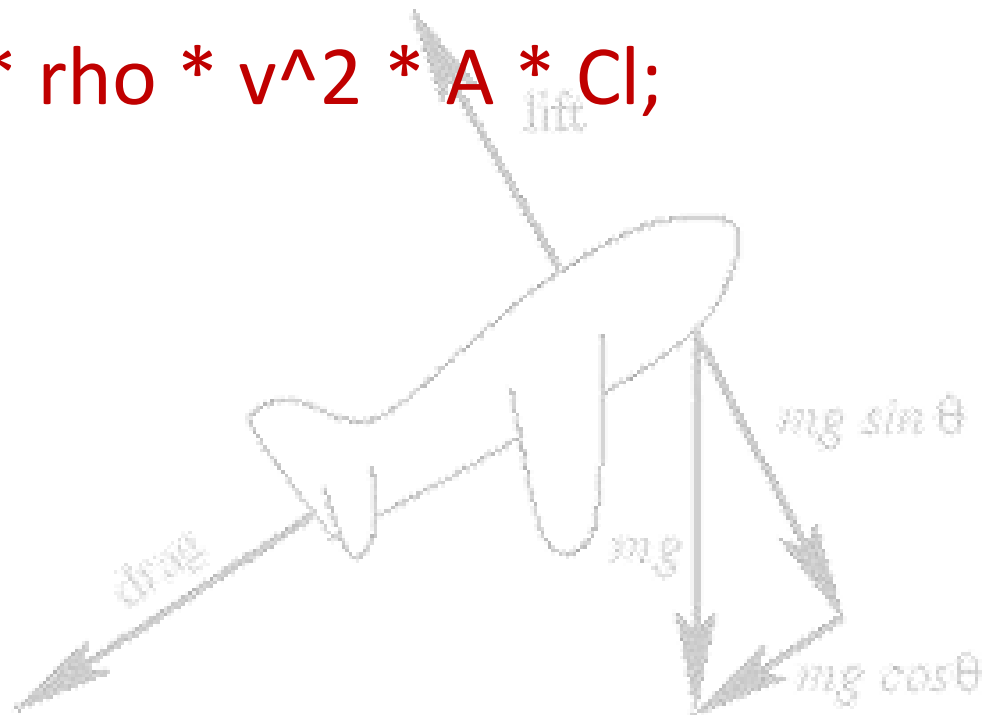
Let's build a **Matlab flight simulator**

- $Cl = 2 * pi * alpha;$ % angle of attack



Let's build a **Matlab flight simulator**

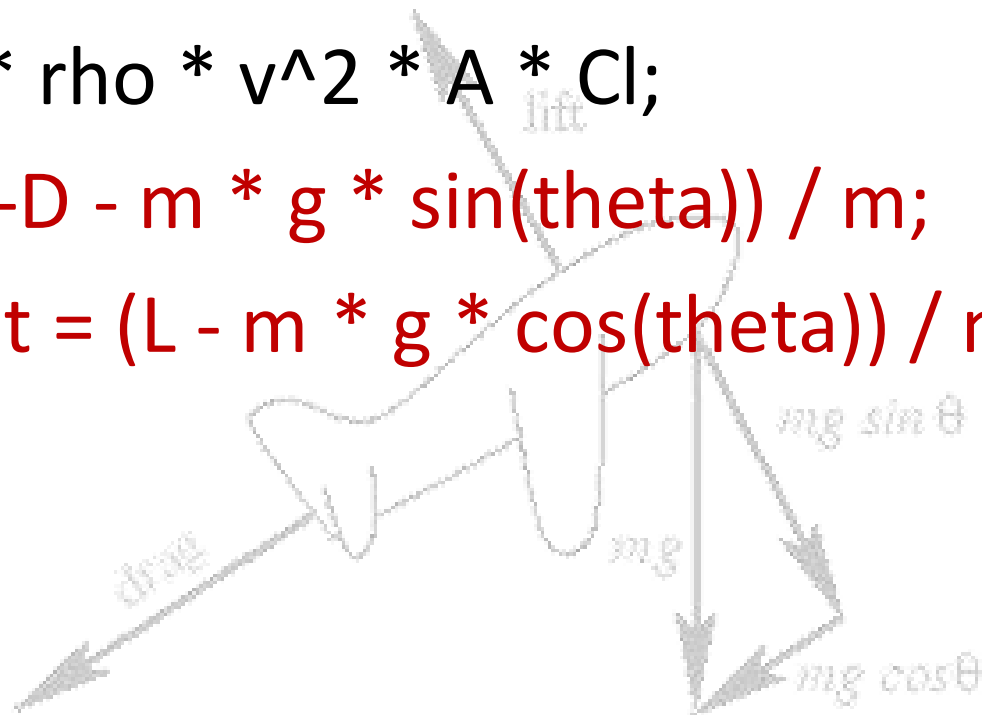
- $C_l = 2 * \pi * \alpha$; % angle of attack
- $D = 0.5 * \rho * v^2 * A * C_d$;
- $L = 0.5 * \rho * v^2 * A * C_l$;



Let's build a **Matlab flight simulator**

Dynamics

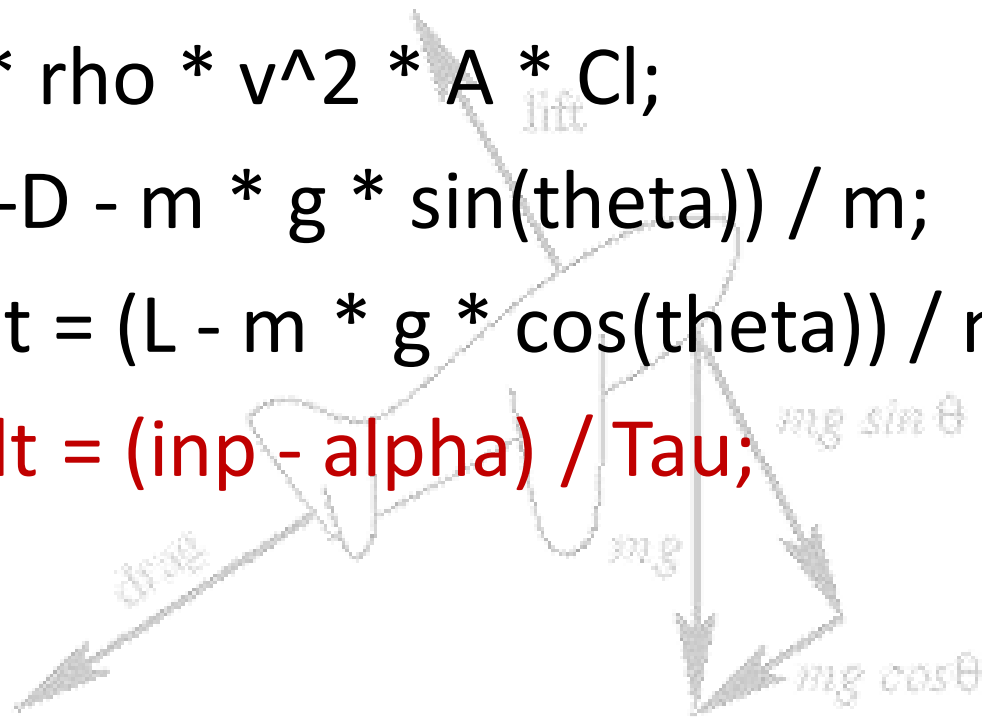
- $Cl = 2 * pi * alpha;$ % angle of attack
- $D = 0.5 * rho * v^2 * A * Cd;$
- $L = 0.5 * rho * v^2 * A * Cl;$
- $dvdt = (-D - m * g * sin(theta)) / m;$
- $dthetadt = (L - m * g * cos(theta)) / m / v;$



Let's build a **Matlab flight simulator**

Elevator trim

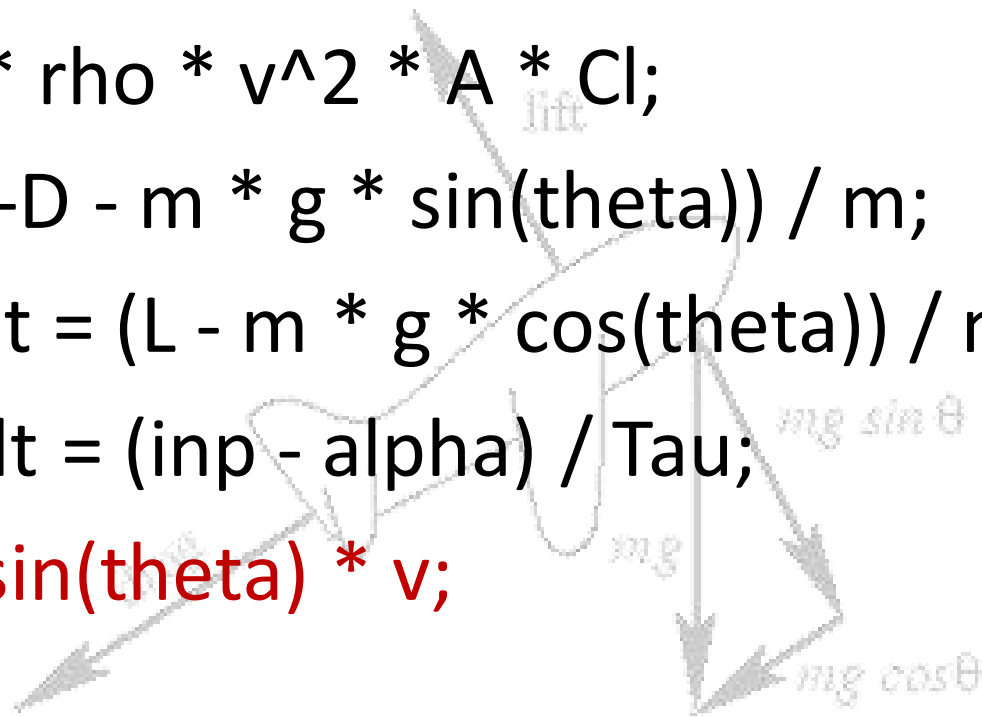
- $Cl = 2 * pi * alpha;$ % angle of attack
- $D = 0.5 * rho * v^2 * A * Cd;$
- $L = 0.5 * rho * v^2 * A * Cl;$
- $dvdt = (-D - m * g * sin(theta)) / m;$
- $dthetadt = (L - m * g * cos(theta)) / m / v;$
- **$dalphadt = (inp - alpha) / Tau;$**



Let's build a **Matlab flight simulator**

Altitude

- $Cl = 2 * pi * alpha;$ % angle of attack
- $D = 0.5 * rho * v^2 * A * Cd;$
- $L = 0.5 * rho * v^2 * A * Cl;$
- $dvdt = (-D - m * g * sin(theta)) / m;$
- $dthetadt = (L - m * g * cos(theta)) / m / v;$
- $dalphadt = (inp - alpha) / Tau;$
- **$dhdt = sin(theta) * v;$**



Eigenvalues of the linearized system

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