

Lecture 1

Fall, 03

Sept 3, 03. ①

- A> Course Admin
- B> Topics / Context
- C> Kinematic Components

Rm 33-319.
MWF - 9-10

- A> Admin
 - MWF 9-10
 - No quiz, No final
 - Grading on P-Setó - 7-8, 2 major ones
 - Group discussion O.K
 - Refs for class

B> Topics / Context put in readings: Batch 78-87, White 16-22

Look at flow regimes using non-dim. parameters

a> $Ka = \frac{x}{L}$

x = mean free path
 L = characteristic length

$Ka \gg 1 \Rightarrow$ Discrete flow, ionized

$Ka \ll 1 \Rightarrow$ Continuum flow

b> $Ma = \frac{V}{c}$

$Ma \ll 1 \Rightarrow$ Incompressible, ρ - const

$Ma \approx 1 \Rightarrow$ Compressible, ρ - variable

Focus on incompressible flows + compressibility correction

c> $k = \frac{\omega L}{V}$ = non-dimension or reduced frequency.

$k \ll 1 \Rightarrow$ steady flow

$$d) Re = \frac{VL}{\nu}$$

$$\nu = \mu/\rho$$

$$Re = \frac{\text{dynamic momentum flux}}{\text{shear stress}}$$

$$\sim \frac{\rho V^2}{\mu \left(\frac{V}{L}\right)}$$

$Re \ll 1$ — Stokes flow

≈ 1 — Oseen flow

$\gg 1$ — High Reynolds # flow
(thin shear + viscous outer flow)

∞ — Turbulent

From kinetic theory

$$\mu \sim \frac{1}{2} \rho \bar{a} \lambda \quad \bar{a} \sim c \text{ (speed of sound)}$$

$$Re \sim \frac{\rho V L}{\frac{1}{2} \rho c \lambda} \sim M \left(\frac{L}{\lambda}\right) \gg 1$$

$$\therefore \frac{M}{Re} \sim \frac{\lambda}{L} \ll 1$$

$M \ll Re$ (low Re , high/low Mach,
continuum assumptions
breaks down)

In addition

$\delta \sim$ B.L. thickness

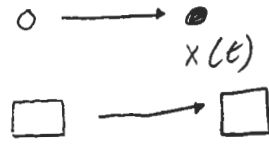
$$\frac{\lambda}{\delta} \sim \frac{\lambda}{L} \cdot \frac{L}{\delta} \ll 1 \quad \frac{L}{\delta} \sim \sqrt{Re}$$

$$\therefore \frac{M}{Re} \sqrt{Re} \ll 1 \quad \Rightarrow \quad \frac{M}{\sqrt{Re}} \ll 1 \quad \text{thin layer}$$

C) Kinematic Components

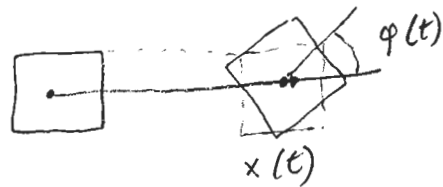
a) Hierarchy of kinematics - Increasing level of complexity of motion

1) Point-mass motion:
(rigid-body translation)



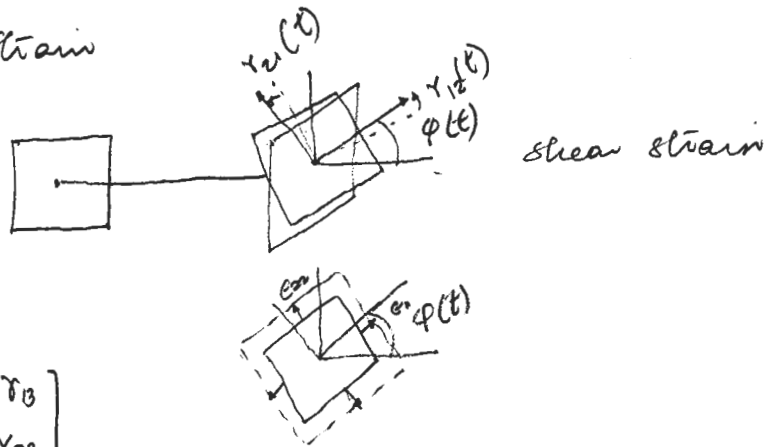
velocity $w(t) = \dot{x}(t)$
 acceleration $a(t) = \dot{w}(t) = \ddot{x}(t)$

2) Rigid-body motion:
translation + rotation

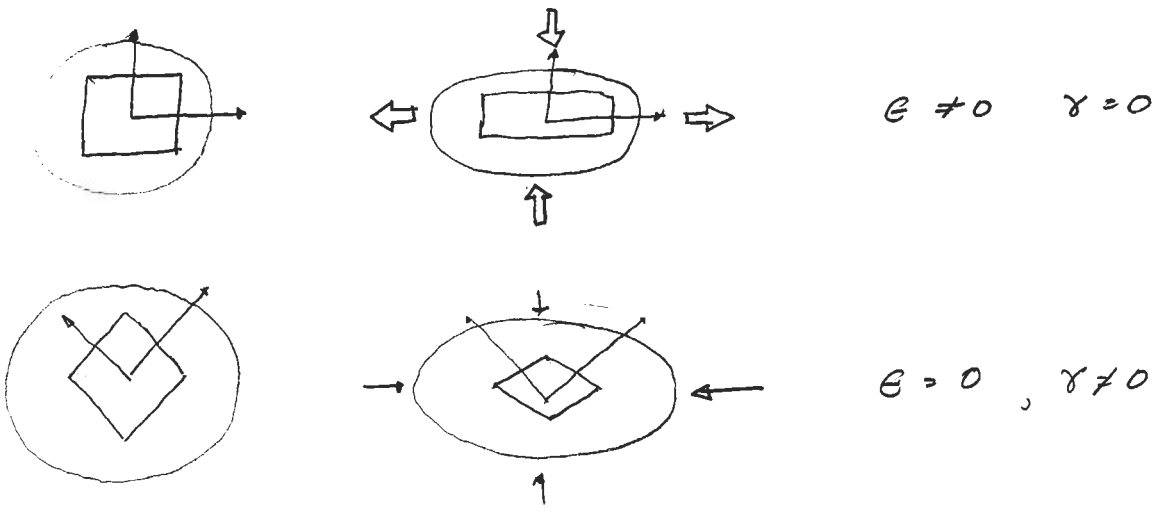


additional: $\Omega = \dot{\phi}(t)$
 $\alpha = \dot{\Omega}(t)$

3) Deformable-body motion:
trans. + rotation + strain



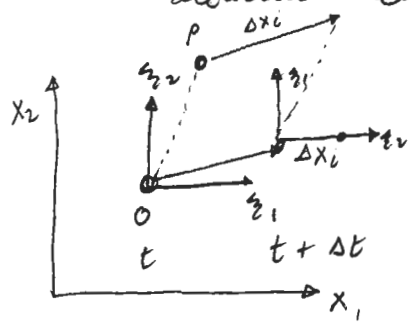
strain tensor =
$$\begin{bmatrix} \epsilon_{11} & \gamma_{12} & \gamma_{13} \\ \gamma_{21} & \epsilon_{22} & \gamma_{23} \\ \gamma_{31} & \gamma_{32} & \epsilon_{33} \end{bmatrix}$$



Whether a strain is a shear or a normal strain depends on orientation of reference axis

0) 0) Kinematic Components (convection + vorticity + strain rate)

Examine linear displacements of two points O and P attached to material. Define material axes ξ_i



$$X_i(\xi_i; t)$$

$$\Delta X_i^P = \Delta X_i^O + \frac{\partial \Delta X_i^P}{\partial \xi_j} \xi_j + \text{HOT}$$

$$a_{ij} = \frac{\partial \Delta X_i}{\partial \xi_j} \text{ (drop?)}$$

Useful to write as

$$= \frac{a_{ij} - a_{ji}}{2} + \frac{a_{ij} + a_{ji}}{2}$$

$$a_{ij} = \phi_{ij} + s_{ij}$$

\uparrow anti sym \uparrow symmetric

$$\therefore \Delta X_i^P = \Delta X_i^O + \phi_{ij} \xi_j + s_{ij} \xi_j$$

On vector notation $\Delta \vec{X}^P = \Delta \vec{X}^O + \bar{a} \cdot \vec{\xi}$, where $\bar{a} = \bar{\phi} + \bar{s}$

Introduce linear dependence

$$\Delta X_i = u_i \Delta t$$

$$\phi_{ij} = 1/2 \omega_{ij} \Delta t$$

$$s_{ij} = e_{ij} \Delta t$$

$$\Rightarrow u_i^P = u_i^O + 1/2 \omega_{ij} \xi_j + e_{ij} \xi_j$$

$\frac{\partial u_i}{\partial z_j} = \frac{1}{2} \omega_{ij} + e_{ij}$
 angular rotation

where $\omega_{ij} \equiv \frac{\partial u_i}{\partial z_j} - \frac{\partial u_j}{\partial z_i}$
 $e_{ij} \equiv \frac{1}{2} \left(\frac{\partial u_i}{\partial z_j} + \frac{\partial u_j}{\partial z_i} \right)$
 follows from p 2 5

$\frac{\partial u_i}{\partial z_j} = \nabla \vec{u} = \begin{bmatrix} & & \\ & 3 \times 3 & \\ & & \end{bmatrix}$
 $\vec{\omega} = \begin{bmatrix} 0 & \cdot & \cdot \\ - & 0 & \cdot \\ - & - & 0 \end{bmatrix}$ - antisymmetric

$\vec{e} = \begin{bmatrix} \cdot & + & + \\ + & \cdot & + \\ + & + & \cdot \end{bmatrix}$ - symmetric

$\vec{\omega} = \begin{bmatrix} 0 & -\omega_z & \omega_y \\ \omega_z & 0 & \omega_x \\ -\omega_y & -\omega_x & 0 \end{bmatrix}$, $\vec{\omega} \cdot \vec{z} = \vec{\omega} \times \frac{\vec{z}}{z}$,

In 2D.

$\omega_x = \omega_y = 0$
 $\omega_z = \frac{\partial v_2}{\partial z_1} - \frac{\partial u_1}{\partial z_2}$

$\therefore \nabla \vec{u} = \begin{bmatrix} \frac{\partial u_1}{\partial z_1} & \frac{\partial u_1}{\partial z_2} \\ \frac{\partial u_2}{\partial z_1} & \frac{\partial u_2}{\partial z_2} \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 0 & -\left(\frac{\partial u_2}{\partial z_1} - \frac{\partial u_1}{\partial z_2}\right) \\ \left(\frac{\partial u_2}{\partial z_1} - \frac{\partial u_1}{\partial z_2}\right) & 0 \end{bmatrix}$
 $+ \begin{bmatrix} \frac{\partial u_1}{\partial z_1} & \frac{1}{2} \left(\frac{\partial u_1}{\partial z_2} + \frac{\partial u_2}{\partial z_1}\right) \\ \frac{1}{2} \left(\frac{\partial u_1}{\partial z_2} + \frac{\partial u_2}{\partial z_1}\right) & \frac{\partial u_2}{\partial z_2} \end{bmatrix}$

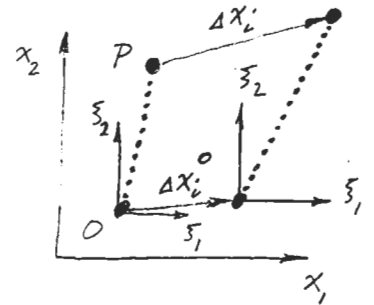


KINEMATIC COMPONENTS

Linear displacements of two points O and P are related by

$$\Delta x_i = \Delta x_i^0 + \frac{\partial(\Delta x_i)}{\partial \xi_j} \xi_j \quad \xi_i = \overrightarrow{PO}$$

local coordinate



define $\frac{\partial(\Delta x_i)}{\partial \xi_j} = a_{ij}$ displacement-gradient tensor

↙ symmetric

↘ antisymmetric

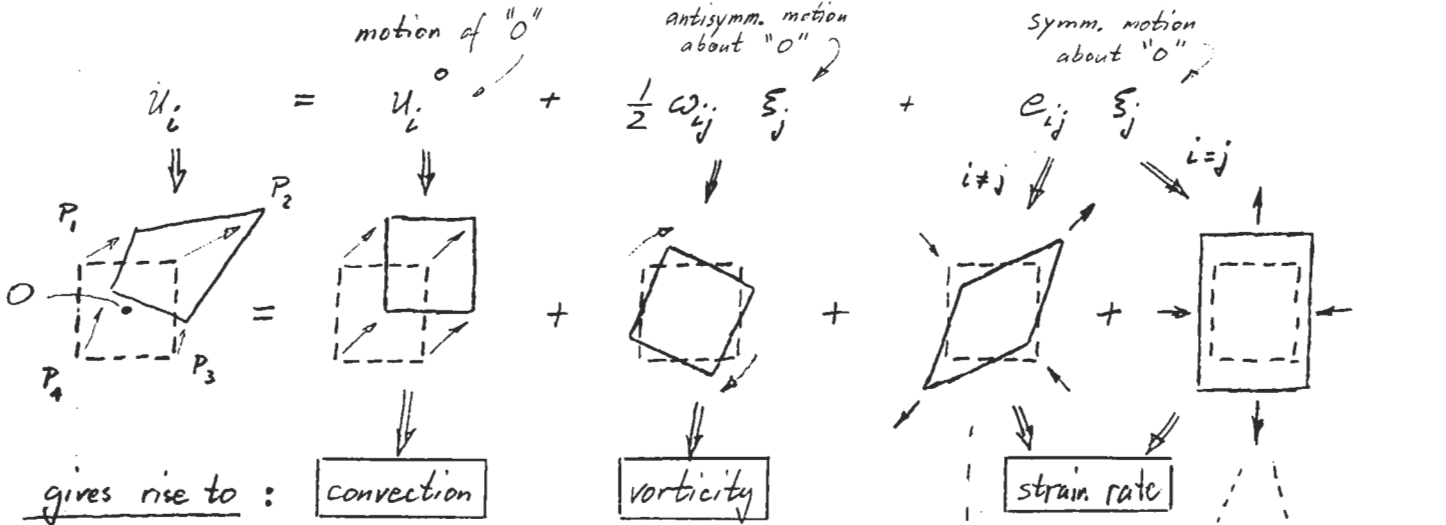
$$s_{ij} = \frac{a_{ij} + a_{ji}}{2}$$

$$\varphi_{ij} = \frac{a_{ij} - a_{ji}}{2}$$

so that $a_{ij} = s_{ij} + \varphi_{ij}$

$$\Delta x_i = \Delta x_i^0 + \varphi_{ij} \xi_j + s_{ij} \xi_j$$

Introduce time dependence: $\Delta x_i = u_i \Delta t$, $\varphi_{ij} = \frac{1}{2} \omega_{ij} \Delta t$, $s_{ij} = e_{ij} \Delta t$



All these components are related to the velocity field