

6. Vector Integral Calculus in Space

6A. Vector Fields in Space

- 6A-1** a) the vectors are all unit vectors, pointing radially outward.
 b) the vector at P has its head on the y -axis, and is perpendicular to it

6A-2 $\frac{1}{2}(-x\mathbf{i} - y\mathbf{j} - z\mathbf{k})$

6A-3 $\omega(-z\mathbf{j} + y\mathbf{k})$

6A-4 A vector field $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + P\mathbf{k}$ is parallel to the plane $3x - 4y + z = 2$ if it is perpendicular to the normal vector to the plane, $3\mathbf{i} - 4\mathbf{j} + \mathbf{k}$: the condition on M, N, P therefore is $3M - 4N + P = 0$, or $P = 4N - 3M$.

The most general such field is therefore $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + (4N - 3M)\mathbf{k}$, where M and N are functions of x, y, z .

6B. Surface Integrals and Flux

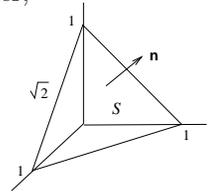
6B-1 We have $\mathbf{n} = \frac{x\mathbf{i} + y\mathbf{j} + z\mathbf{k}}{a}$; therefore $\mathbf{F} \cdot \mathbf{n} = a$.

$$\text{Flux through } S = \iint_S \mathbf{F} \cdot \mathbf{n} dS = a(\text{area of } S) = 4\pi a^3.$$

6B-2 Since \mathbf{k} is parallel to the surface, the field is everywhere tangent to the cylinder, hence the flux is 0.

6B-3 $\frac{\mathbf{i} + \mathbf{j} + \mathbf{k}}{\sqrt{3}}$ is a normal vector to the plane, so $\mathbf{F} \cdot \mathbf{n} = \frac{1}{\sqrt{3}}$.

$$\text{Therefore, flux} = \frac{\text{area of region}}{\sqrt{3}} = \frac{\frac{1}{2}(\text{base})(\text{height})}{\sqrt{3}} = \frac{\frac{1}{2}(\sqrt{2})(\frac{\sqrt{3}}{2}\sqrt{2})}{\sqrt{3}} = \frac{1}{2}.$$



6B-4 $\mathbf{n} = \frac{x\mathbf{i} + y\mathbf{j} + z\mathbf{k}}{a}$; $\mathbf{F} \cdot \mathbf{n} = \frac{y^2}{a}$. Calculating in spherical coordinates,

$$\text{flux} = \iint_S \frac{y^2}{a} dS = \frac{1}{a} \int_0^\pi \int_0^\pi a^4 \sin^3 \phi \sin^2 \theta d\phi d\theta = a^3 \int_0^\pi \int_0^\pi \sin^3 \phi \sin^2 \theta d\phi d\theta.$$

$$\text{Inner integral: } \left[\sin^2 \theta (-\cos \phi + \frac{1}{3} \cos^3 \phi) \right]_0^\pi = \frac{4}{3} \sin^2 \theta;$$

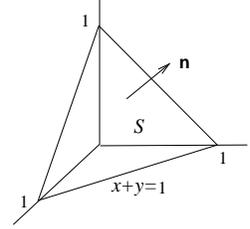
$$\text{Outer integral: } \left[\frac{4}{3} a^3 (\frac{1}{2} \theta - \frac{1}{4} \sin 2\theta) \right]_0^\pi = \frac{2}{3} \pi a^3.$$

$$\mathbf{6B-5} \quad \mathbf{n} = \frac{\mathbf{i} + \mathbf{j} + \mathbf{k}}{\sqrt{3}}; \quad \mathbf{F} \cdot \mathbf{n} = \frac{z}{\sqrt{3}}.$$

$$\text{flux} = \iint_S \frac{z}{\sqrt{3}} \frac{dx dy}{|\mathbf{n} \cdot \mathbf{k}|} = \frac{1}{\sqrt{3}} \iint_S (1-x-y) \frac{dx dy}{1/\sqrt{3}} = \int_0^1 \int_0^{1-y} (1-x-y) dx dy.$$

$$\text{Inner integral: } = x - \frac{1}{2}x^2 - xy \Big|_0^{1-y} = \frac{1}{2}(1-y)^2.$$

$$\text{Outer integral: } = \int_0^1 \frac{1}{2}(1-y)^2 dy = \frac{1}{2} \cdot -\frac{1}{3} \cdot (1-y)^3 \Big|_0^1 = \frac{1}{6}.$$



6B-6 $z = f(x, y) = x^2 + y^2$ (a paraboloid). By (13) in Notes V9,

$$d\mathbf{S} = (-2x \mathbf{i} - 2y \mathbf{j} + \mathbf{k}) dx dy.$$

(This points generally “up”, since the \mathbf{k} component is positive.) Since $\mathbf{F} = x \mathbf{i} + y \mathbf{j} + z \mathbf{k}$,

$$\iint_S \mathbf{F} \cdot d\mathbf{S} = \iint_R (-2x^2 - 2y^2 + z) dx dy,$$

where R is the interior of the unit circle in the xy -plane, i.e., the projection of S onto the xy -plane). Since $z = x^2 + y^2$, the above integral

$$= - \iint_R (x^2 + y^2) dx dy = - \int_0^{2\pi} \int_0^1 r^2 \cdot r dr d\theta = -2\pi \cdot \frac{1}{4} = -\frac{\pi}{2}.$$

The answer is negative since the positive direction for flux is that of \mathbf{n} , which here points into the inside of the paraboloidal cup, whereas the flow $x \mathbf{i} + y \mathbf{j} + z \mathbf{k}$ is generally from the inside toward the outside of the cup, i.e., in the opposite direction.

$$\mathbf{6B-8} \quad \text{On the cylindrical surface, } \mathbf{n} = \frac{x \mathbf{i} + y \mathbf{j}}{a}, \quad \mathbf{F} \cdot \mathbf{n} = \frac{y^2}{a}.$$

In cylindrical coordinates, since $y = a \sin \theta$, this gives us $\mathbf{F} \cdot d\mathbf{S} = \mathbf{F} \cdot \mathbf{n} dS = a^2 \sin^2 \theta dz d\theta$.

$$\text{Flux} = \int_{-\pi/2}^{\pi/2} \int_0^k a^2 \sin^2 \theta dz d\theta = a^2 h \int_{-\pi/2}^{\pi/2} \sin^2 \theta d\theta = a^2 h \left(\frac{\theta}{2} - \frac{\sin 2\theta}{4} \right) \Big|_{-\pi/2}^{\pi/2} = \frac{\pi}{2} a^2 h.$$

6B-12 Since the distance from a point $(x, y, 0)$ up to the hemispherical surface is z ,

$$\text{average distance} = \frac{\iint_S z dS}{\iint_S dS}.$$

In spherical coordinates, $\iint_S z dS = \int_0^{2\pi} \int_0^{\pi/2} a \cos \phi \cdot a^2 \sin \phi d\phi d\theta$.

$$\text{Inner: } = a^3 \int_0^{\pi/2} \sin \phi \cos \phi d\phi = a^3 \left(\frac{\sin^2 \phi}{2} \right) \Big|_0^{\pi/2} = \frac{a^3}{2}. \quad \text{Outer: } = \frac{a^3}{2} \int_0^{2\pi} d\theta = \pi a^3.$$

Finally, $\iint_S dS = \text{area of hemisphere} = 2\pi a^2$, so average distance $= \frac{\pi a^3}{2\pi a^2} = \frac{a}{2}$.

6C. Divergence Theorem

6C-1a $\operatorname{div} \mathbf{F} = M_x + N_y + P_z = 2xy + x + x = 2x(y + 1).$

6C-2 Using the product and chain rules for the first, symmetry for the others,

$$(\rho^n x)_x = n\rho^{n-1} \frac{x}{\rho} + \rho^n, \quad (\rho^n y)_y = n\rho^{n-1} \frac{y}{\rho} + \rho^n, \quad (\rho^n z)_z = n\rho^{n-1} \frac{z}{\rho} + \rho^n;$$

adding these three, we get $\operatorname{div} \mathbf{F} = n\rho^{n-1} \frac{x^2 + y^2 + z^2}{\rho} + 3\rho^n = \rho^n(n + 3).$

Therefore, $\operatorname{div} \mathbf{F} = 0 \Leftrightarrow n = -3.$

6C-3 Evaluating the triple integral first, we have $\operatorname{div} \mathbf{F} = 3$, therefore

$$\iiint_D \operatorname{div} \mathbf{F} dV = 3(\operatorname{vol. of } D) = 3 \frac{2}{3} \pi a^3 = 2\pi a^3.$$

To evaluate the double integral over the closed surface $S_1 + S_2$, the normal vectors are:

$$\mathbf{n}_1 = \frac{x\mathbf{i} + y\mathbf{j} + z\mathbf{k}}{a} \quad (\text{hemisphere } S_1), \quad \mathbf{n}_2 = -\mathbf{k} \quad (\text{disc } S_2);$$

using these, the surface integral for the flux through S is

$$\iint_S \mathbf{F} \cdot d\mathbf{S} = \iint_{S_1} \frac{x^2 + y^2 + z^2}{a} dS + \iint_{S_2} -z dS = \iint_{S_1} a dS,$$

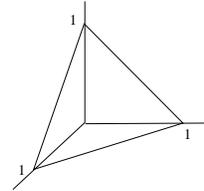
since $x^2 + y^2 + z^2 = \rho^2 = a^2$ on S_1 , and $z = 0$ on S_2 . So the value of the surface integral is

$$a(\operatorname{area of } S_1) = a(2\pi a^2) = 2\pi a^3,$$

which agrees with the triple integral above.

6C-5 The divergence theorem says $\iint_S \mathbf{F} \cdot d\mathbf{S} = \iiint_D \operatorname{div} \mathbf{F} dV.$

Here $\operatorname{div} \mathbf{F} = 1$, so that the right-hand integral is just the volume of the tetrahedron, which is $\frac{1}{3}(\text{base})(\text{height}) = \frac{1}{3}(\frac{1}{2})(1) = \frac{1}{6}.$



6C-6 The divergence theorem says $\iint_S \mathbf{F} \cdot d\mathbf{S} = \iiint_D \operatorname{div} \mathbf{F} dV.$

Here $\operatorname{div} \mathbf{F} = 1$, so the right-hand integral is the volume of the solid cone, which has height 1 and base radius 1; its volume is $\frac{1}{3}(\text{base})(\text{height}) = \pi/3.$

6C-7a Evaluating the triple integral first, over the cylindrical solid D , we have

$$\operatorname{div} \mathbf{F} = 2x + x = 3x; \quad \iiint_D 3x dV = 0,$$

since the solid is symmetric with respect to the yz -plane. (Physically, assuming the density is 1, the integral has the value \bar{x} (mass of D), where \bar{x} is the x -coordinate of the center of mass; this must be in the yz plane since the solid is symmetric with respect to this plane.)

To evaluate the double integral, note that \mathbf{F} has no \mathbf{k} -component, so there is no flux across the two disc-like ends of the solid. To find the flux across the cylindrical side,

$$\mathbf{n} = x\mathbf{i} + y\mathbf{j}, \quad \mathbf{F} \cdot \mathbf{n} = x^3 + xy^2 = x^3 + x(1 - x^2) = x,$$

since the cylinder has radius 1 and equation $x^2 + y^2 = 1$. Thus

$$\iint_S x \, dS = \int_0^{2\pi} \int_0^1 \cos \theta \, dz \, d\theta = \int_0^{2\pi} \cos \theta \, d\theta = 0.$$

6C-8 a) Reorient the lower hemisphere S_2 by reversing its normal vector; call the reoriented surface S'_2 . Then $S = S_1 + S'_2$ is a closed surface, with the normal vector pointing outward everywhere, so by the divergence theorem,

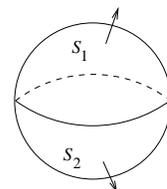
$$\iint_S \mathbf{F} \cdot d\mathbf{S} = \iint_{S_1} \mathbf{F} \cdot d\mathbf{S} + \iint_{S'_2} \mathbf{F} \cdot d\mathbf{S} = \iiint_D \operatorname{div} \mathbf{F} \, dV = 0,$$

since by hypothesis $\operatorname{div} \mathbf{F} = 0$. The above shows

$$\iint_{S_1} \mathbf{F} \cdot d\mathbf{S} = - \iint_{S'_2} \mathbf{F} \cdot d\mathbf{S} = \iint_{S_2} \mathbf{F} \cdot d\mathbf{S},$$

since reversing the orientation of a surface changes the sign of the flux through it.

b) The same statement holds if S_1 and S_2 are two oriented surfaces having the same boundary curve, but not intersecting anywhere else, and oriented so that S_1 and S'_2 (i.e., S_2 with its orientation reversed) together make up a closed surface S with outward-pointing normal.



6C-10 If $\operatorname{div} \mathbf{F} = 0$, then for any closed surface S , we have by the divergence theorem

$$\iint_S \mathbf{F} \cdot d\mathbf{S} = \iiint_D \operatorname{div} \mathbf{F} \, dV = 0.$$

Conversely: $\iint_S \mathbf{F} \cdot d\mathbf{S} = 0$ for every closed surface $S \Rightarrow \operatorname{div} \mathbf{F} = 0$.

For suppose there were a point P_0 at which $(\operatorname{div} \mathbf{F})_0 \neq 0$ — say $(\operatorname{div} \mathbf{F})_0 > 0$. Then by continuity, $\operatorname{div} \mathbf{F} > 0$ in a very small spherical ball D surrounding P_0 , so that by the divergence theorem (S is the surface of the ball D),

$$\iint_S \mathbf{F} \cdot d\mathbf{S} = \iiint_D \operatorname{div} \mathbf{F} \, dV > 0.$$

But this contradicts our hypothesis that $\iint_S \mathbf{F} \cdot d\mathbf{S} = 0$ for every closed surface S .

6C-11 flux of $\mathbf{F} = \iint_S \mathbf{F} \cdot d\mathbf{n} = \iiint_D \operatorname{div} \mathbf{F} \, dV = \iiint_D 3 \, dV = 3(\text{vol. of } D)$.

6D. Line Integrals in Space

6D-1 a) $C: x = t, dx = dt; y = t^2, dy = 2t \, dt; z = t^3, dz = 3t^2 \, dt;$

$$\begin{aligned} \int_C y \, dx + z \, dy - x \, dz &= \int_0^1 (t^2) \, dt + t^3(2t \, dt) - t(3t^2 \, dt) \\ &= \int_0^1 (t^2 + 2t^4 - 3t^3) \, dt = \left. \frac{t^3}{3} + \frac{2t^5}{5} - \frac{3t^4}{4} \right|_0^1 = \frac{1}{3} + \frac{2}{5} - \frac{3}{4} = -\frac{1}{60}. \end{aligned}$$

b) $C: x = t, y = t, z = t; \int_C y \, dx + z \, dy - x \, dz = \int_0^1 t \, dt = \frac{1}{2}.$

c) $C = C_1 + C_2 + C_3$; $C_1 : y = z = 0$; $C_2 : x = 1, z = 0$; $C_3 : x = 1, y = 1$

$$\int_C y dx + z dy - x dz = \int_{C_1} 0 + \int_{C_2} 0 + \int_0^1 -dz = -1.$$

d) $C : x = \cos t, y = \sin t, z = t$; $\int_C zx dx + zy dy + x dz$

$$= \int_0^{2\pi} t \cos t (-\sin t dt) + t \sin t (\cos t dt) + \cos t dt = \int_0^{2\pi} \cos t dt = 0.$$

6D-2 The field \mathbf{F} is always pointed radially outward; if C lies on a sphere centered at the origin, its unit tangent \mathbf{t} is always tangent to the sphere, therefore perpendicular to the radius; this means $\mathbf{F} \cdot \mathbf{t} = 0$ at every point of C . Thus $\int_C \mathbf{F} \cdot d\mathbf{r} = \int_C \mathbf{F} \cdot \mathbf{t} ds = 0$.

6D-4 a) $\mathbf{F} = \nabla f = 2x \mathbf{i} + 2y \mathbf{j} + 2z \mathbf{k}$.

b) (i) Directly, letting C be the helix: $x = \cos t, y = \sin t, z = t$, from $t = 0$ to $t = 2n\pi$,

$$\int_C M dx + N dy + P dz = \int_0^{2n\pi} 2 \cos t (-\sin t) dt + 2 \sin t (\cos t) dt + 2t dt = \int_0^{2n\pi} 2t dt = (2n\pi)^2.$$

b) (ii) Choose the vertical path $x = 1, y = 0, z = t$; then

$$\int_C M dx + N dy + P dz = \int_0^{2n\pi} 2t dt = (2n\pi)^2.$$

b) (iii) By the First Fundamental Theorem for line integrals,

$$\int_C \mathbf{F} \cdot d\mathbf{r} = f(1, 0, 2n\pi) - f(1, 0, 0) = 91^2 + (2n\pi)^2 - 1^2 = (2n\pi)^2$$

6D-5 By the First Fundamental Theorem for line integrals,

$$\int_C \mathbf{F} \cdot d\mathbf{r} = \sin(xyz) \Big|_Q - \sin(xyz) \Big|_P,$$

where C is any path joining P to Q . The maximum value of this difference is $1 - (-1) = 2$, since $\sin(xyz)$ ranges between -1 and 1 .

For example, any path C connecting $P : (1, 1, -\pi/2)$ to $Q : (1, 1, \pi/2)$ will give this maximum value of 2 for $\int_C \mathbf{F} \cdot d\mathbf{r}$.

6E. Gradient Fields in Space

6E-1 a) Since $M = x^2, N = y^2, P = z^2$ are continuously differentiable, the differential is exact because $N_z = P_y = 0, M_z = P_x = 0, M_y = N_x = 0$; $f(x, y, z) = (x^3 + y^3 + z^3)/3$.

b) Exact: M, N, P are continuously differentiable for all x, y, z , and

$$N_z = P_y = 2xy, \quad M_z = P_x = y^2, \quad M_y = N_x = 2yz; \quad f(x, y, z) = xy^2.$$

c) Exact: M, N, P are continuously differentiable for all x, y, z , and

$$N_z = P_y = x, \quad M_z = P_x = y, \quad M_y = N_x = 6x^2 + z; \quad f(x, y, z) = 2x^3y + xyz.$$

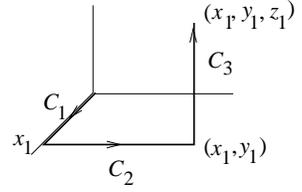
6E-2 $\text{curl } \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \partial_x & \partial_y & \partial_z \\ x^2y & yz & xyz^2 \end{vmatrix} = (xz^2 - y) \mathbf{i} - yz^2 \mathbf{j} - x^2 \mathbf{k}.$

6E-3 a) It is easily checked that $\text{curl } \mathbf{F} = 0$.

b) (i) using method I:

$$\begin{aligned} f(x_1, y_1, z_1) &= \int_{(0,0,0)}^{(x_1, y_1, z_1)} \mathbf{F} \cdot d\mathbf{r} = \int_{C_1} \mathbf{F} \cdot d\mathbf{r} + \int_{C_2} \mathbf{F} \cdot d\mathbf{r} + \int_{C_3} \mathbf{F} \cdot d\mathbf{r} \\ &= \int_0^{x_1} x \, dx + \int_0^{y_1} y \, dy + \int_0^{z_1} z \, dz = \frac{1}{2}x_1^2 + \frac{1}{2}y_1^2 + \frac{1}{2}z_1^2. \end{aligned}$$

Therefore $f(x, y, z) = \frac{1}{2}(x^2 + y^2 + z^2) + c$.



(ii) Using method II: We seek $f(x, y, z)$ such that $f_x = 2xy + z$, $f_y = x^2$, $f_z = x$.

$$\begin{aligned} f_x = 2xy + z &\Rightarrow f = x^2y + xz + g(y, z). \\ f_y = x^2 + g_y = x^2 &\Rightarrow g_y = 0 \Rightarrow g = h(z) \\ f_z = x + h'(z) = x &\Rightarrow h' = 0 \Rightarrow h = c \end{aligned}$$

Therefore $f(x, y, z) = x^2y + xz + c$.

(iii) If $f_x = yz$, $f_y = xz$, $f_z = xy$, then by inspection, $f(x, y, z) = xyz + c$.

6E-4 Let $F = f - g$. Since ∇ is a linear operator, $\nabla F = \nabla f - \nabla g = \mathbf{0}$

We now show: $\nabla F = \mathbf{0} \Rightarrow F = c$.

Fix a point $P_0 : (x_0, y_0, z_0)$. Then by the Fundamental Theorem for line integrals,

$$F(P) - F(P_0) = \int_{P_0}^P \nabla F \cdot d\mathbf{r} = 0.$$

Therefore $F(P) = F(P_0)$ for all P , i.e., $F(x, y, z) = F(x_0, y_0, z_0) = c$.

6E-5 \mathbf{F} is a gradient field only if these equations are satisfied:

$$N_z = P_y : 2xz + ay = bxz + 2y \quad M_z = P_x : 2yz = byz \quad M_y = N_x : z^2 = z^2.$$

Thus the conditions are: $a = 2$, $b = 2$.

Using these values of a and b we employ Method 2 to find the potential function f :

$$\begin{aligned} f_x = yz^2 &\Rightarrow f = xyz^2 + g(y, z); \\ f_y = xz^2 + g_y = xz^2 + 2yz &\Rightarrow g_y = 2yz \Rightarrow g = y^2z + h(z) \\ f_z = 2xyz + y^2 + h'(z) = 2xyz + y^2 &\Rightarrow h = c; \end{aligned}$$

therefore, $f(x, y, z) = xyz^2 + y^2z + c$.

6E-6 a) $Mdx + Ndy + Pdz$ is an exact differential if there exists some function $f(x, y, z)$ for which $df = Mdx + Ndy + Pdz$; that is, for which $f_x = M$, $f_y = N$, $f_z = P$.

b) The given differential is exact if the following equations are satisfied:

$$\begin{aligned} N_z = P_y : (a/2)x^2 + 6xy^2z + 3byz^2 &= 3x^2 + 3cxy^2z + 12yz^2; \\ M_z = P_x : axy + 2y^3z &= 6xy + cy^3z \\ M_y = N_x : axz + 3y^2z^2 &= axz + 3y^2z^2. \end{aligned}$$

Solving these, we find that the differential is exact if $a = 6$, $b = 4$, $c = 2$.

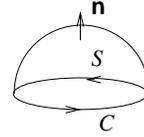
c) We find $f(x, y, z)$ using method 2:

$$\begin{aligned} f_x = 6xyz + y^3z^2 &\Rightarrow f = 3x^2yz + xy^3z^2 + g(y, z); \\ f_y = 3x^2z + 3xy^2z^2 + g_y = 3x^2z + 3xy^2z^2 + 4yz^3 &\Rightarrow g_y = 4yz^3 \Rightarrow g = 2y^2z^3 + h(z) \\ f_z = 3x^2y + 2xy^3z + 6y^2z^2 + h'(z) = 3x^2y + 2xy^3z + 6y^2z^2 &\Rightarrow h'(z) = 0 \Rightarrow h = c. \end{aligned}$$

Therefore, $f(x, y, z) = 3x^2yz + xy^3z^2 + 2y^2z^3 + c$.

6F. Stokes' Theorem

6F-1 a) For the line integral, $\oint_C \mathbf{F} \cdot d\mathbf{r} = \oint_C xdx + ydy + zdz = 0$, since the differential is exact.



For the surface integral, $\nabla \times \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \partial_x & \partial_y & \partial_z \\ x & y & z \end{vmatrix} = \mathbf{0}$, and therefore $\iint_S \nabla \times \mathbf{F} \cdot d\mathbf{S} = 0$.

b) Line integral: $\oint_C ydx + zdy + xdz = \oint_C ydx$, since $z = 0$ and $dz = 0$ on C .

$$\text{Using } x = \cos t, \quad y = \sin t, \quad \int_0^{2\pi} -\sin^2 t dt = -\int_0^{2\pi} \frac{1 - \cos 2t}{2} dt = -\pi.$$

Surface integral: $\text{curl } \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \partial_x & \partial_y & \partial_z \\ y & z & x \end{vmatrix} = -\mathbf{i} - \mathbf{j} - \mathbf{k}; \quad \mathbf{n} = x\mathbf{i} + y\mathbf{j} + z\mathbf{k}$

$$\iint_S \nabla \times \mathbf{F} \cdot \mathbf{n} dS = -\iint_S (x + y + z) dS.$$

To evaluate, we use $x = r \cos \theta$, $y = r \sin \theta$, $z = \rho \cos \phi$. $r = \rho \sin \phi$, $dS = \rho^2 \sin \phi d\phi d\theta$; note that $\rho = 1$ on S . The integral then becomes

$$-\int_0^{2\pi} \int_0^{\pi/2} [\sin \phi (\cos \theta + \sin \theta) + \cos \phi] \sin \phi d\phi d\theta$$

$$\text{Inner: } -\left[(\cos \theta + \sin \theta) \left(\frac{\phi}{2} - \frac{\sin 2\phi}{4} \right) + \frac{1}{2} \sin^2 \phi \right]_0^{\pi/2} = -\left[(\cos \theta + \sin \theta) \frac{\pi}{4} + \frac{1}{2} \right];$$

$$\text{Outer: } \int_0^{2\pi} \left(-\frac{1}{2} - (\cos \theta + \sin \theta) \frac{\pi}{4} \right) d\theta = -\pi.$$

6F-2 The surface S is: $z = -x - y$, so that $f(x, y) = -x - y$.

$$\mathbf{n} dS = \langle -f_x, -f_y, 1 \rangle dx dy = \langle 1, 1, 1 \rangle dx dy.$$

(Note the signs: \mathbf{n} points upwards, and therefore should have a positive k -component.)

$$\text{curl } \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \partial_x & \partial_y & \partial_z \\ y & z & x \end{vmatrix} = -\mathbf{i} - \mathbf{j} - \mathbf{k}$$

Therefore $\iint_S \text{curl } \mathbf{F} \cdot \mathbf{n} dS = -\iint_{S'} 3 dA = -3\pi$, where S' is the projection of S , i.e., the interior of the unit circle in the xy -plane.

As for the line integral, we have C : $x = \cos t$, $y = \sin t$, $z = -\cos t - \sin t$, so that

$$\begin{aligned}\oint_C y dx + z dy + x dz &= \int_0^{2\pi} \left[-\sin^2 t - (\cos^2 t + \sin t \cos t) + \cos t(\sin t - \cos t) \right] dt \\ &= \int_0^{2\pi} (-\sin^2 t - \cos^2 t - \cos^2 t) dt = \int_0^{2\pi} \left[-1 - \frac{1}{2}(1 + \cos 2t) \right] dt = -\frac{3}{2} \cdot 2\pi = -3\pi.\end{aligned}$$

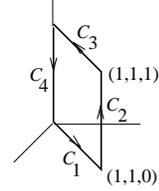
6F-3 Line integral: $\oint_C yz dx + xz dy + xy dz$ over the path $C = C_1 + \dots + C_4$:

$$\int_{C_1} = 0, \quad \text{since } z = dz = 0 \text{ on } C_1;$$

$$\int_{C_2} = \int_0^1 1 \cdot 1 dz = 1, \quad \text{since } x = 1, y = 1, dx = 0, dy = 0 \text{ on } C_2;$$

$$\int_{C_3} y dx + x dy = \int_1^0 x dx + x dx = -1, \quad \text{since } y = x, z = 1, dz = 0 \text{ on } C_3;$$

$$\int_{C_4} = 0, \quad \text{since } x = 0, y = 0 \text{ on } C_4.$$



Adding up, we get $\oint_C \mathbf{F} \cdot d\mathbf{r} = \int_{C_1} + \int_{C_2} + \int_{C_3} + \int_{C_4} = 0$. For the surface integral,

$$\text{curl } \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \partial_x & \partial_y & \partial_z \\ yz & xz & xy \end{vmatrix} = \mathbf{i}(x-x) - \mathbf{j}(y-y) + \mathbf{k}(z-z) = \mathbf{0}; \quad \text{thus } \iint \text{curl } \mathbf{F} \cdot d\mathbf{S} = 0.$$

6F-5 Let S_1 be the top of the cylinder (oriented so $\mathbf{n} = \mathbf{k}$), and S_2 the side.

a) We have $\text{curl } \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \partial_x & \partial_y & \partial_z \\ -y & x & x^2 \end{vmatrix} = -2x\mathbf{j} + 2\mathbf{k}$.

For the top: $\iint_{S_1} \text{curl } \mathbf{F} \cdot \mathbf{n} dS = \iint_{S_1} 2 dS = 2(\text{area of } S_1) = 2\pi a^2$.

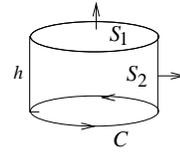
For the side: we have $\mathbf{n} = \frac{x\mathbf{i} + y\mathbf{j}}{a}$, and $dS = dz \cdot a d\theta$, so that

$$\iint_{S_2} \text{curl } \mathbf{F} \cdot \mathbf{n} dS = \int_0^{2\pi} \int_0^h \frac{-2xy}{a} a dz d\theta = \int_0^{2\pi} -2h(a \cos \theta)(a \sin \theta) d\theta = -ha^2 \sin^2 \theta \Big|_0^{2\pi} = 0.$$

Adding, $\iint_S \text{curl } \mathbf{F} \cdot d\mathbf{S} = \iint_{S_1} + \iint_{S_2} = 2\pi a^2$.

b) Let C be the circular boundary of S , parameterized by $x = a \cos \theta$, $y = a \sin \theta$, $z = 0$. Then using Stokes' theorem,

$$\iint_S \text{curl } \mathbf{F} \cdot d\mathbf{S} = \oint_C -y dx + x dy + x^2 dz = \int_0^{2\pi} (a^2 \sin^2 \theta + a^2 \cos^2 \theta) d\theta = 2\pi a^2.$$



6G. Topological Questions

6G-1 a) yes b) no c) yes d) no; yes; no; yes; no; yes

6G-2 Recall that $\rho_x = x/\rho$, etc. Then, using the chain rule,

$$\text{curl } \mathbf{F} = (n\rho^{n-1}z \frac{y}{\rho} - n\rho^{n-1}y \frac{z}{\rho})\mathbf{i} + (n\rho^{n-1}z \frac{x}{\rho} - n\rho^{n-1}x \frac{z}{\rho})\mathbf{j} + (n\rho^{n-1}y \frac{x}{\rho} - n\rho^{n-1}x \frac{y}{\rho})\mathbf{k}.$$

Therefore $\text{curl } \mathbf{F} = \mathbf{0}$. To find the potential function, we let P_0 be any convenient starting point, and integrate along some path to $P_1 : (x_1, y_1, z_1)$. Then, if $n \neq -2$, we have

$$\begin{aligned} \int_C \mathbf{F} \cdot d\mathbf{r} &= \int_{P_0}^{P_1} \rho^n (x dx + y dy + z dz) = \int_{P_0}^{P_1} \rho^n \frac{1}{2} d(\rho^2) \\ &= \int_{P_0}^{P_1} \rho^{n+1} d\rho = \left. \frac{\rho^{n+2}}{n+2} \right]_{P_0}^{P_1} = \frac{\rho_1^{n+2}}{n+2} - \frac{\rho_0^{n+2}}{n+2} = \frac{\rho_1^{n+2}}{n+2} + c, \text{ since } P_0 \text{ is fixed.} \end{aligned}$$

Therefore, we get $\mathbf{F} = \nabla \frac{\rho^{n+2}}{n+2}$, if $n \neq -2$.

If $n = -2$, the line integral becomes $\int_{P_0}^{P_1} \frac{d\rho}{\rho} = \ln \rho_1 + c$, so that $\mathbf{F} = \nabla(\ln \rho)$.

6H. Applications and Further Exercises

6H-1 Let $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + P\mathbf{k}$. By the definition of $\text{curl } \mathbf{F}$, we have

$$\nabla \times \mathbf{F} = (P_y - N_z)\mathbf{i} + (M_z - P_x)\mathbf{j} + (N_x - M_y)\mathbf{k},$$

$$\nabla \cdot (\nabla \times \mathbf{F}) = (P_{yx} - N_{zx}) + (M_{zy} - P_{xy}) + (N_{xz} - M_{yz})$$

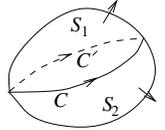
If all the mixed partials exist and are continuous, then $P_{xy} = P_{yx}$, etc. and the right-hand side of the above equation is zero: $\text{div}(\text{curl } \mathbf{F}) = 0$.

6H-2 a) Using the divergence theorem, and the previous problem, (D is the interior of S),

$$\iint_S \text{curl } \mathbf{F} \cdot d\mathbf{S} = \iiint_D \text{div} \text{curl } \mathbf{F} dV = \iiint_D 0 dV = 0.$$

b) Draw a closed curve C on S that divides it into two pieces S_1 and S_2 both having C as boundary. Orient C compatibly with S_1 , then the curve C' obtained by reversing the orientation of C will be oriented compatibly with S_2 . Using Stokes' theorem,

$$\iint_S \text{curl } \mathbf{F} \cdot d\mathbf{S} = \iint_{S_1} \text{curl } \mathbf{F} \cdot d\mathbf{S} + \iint_{S_2} \text{curl } \mathbf{F} \cdot d\mathbf{S} = \oint_C \mathbf{F} \cdot d\mathbf{r} + \oint_{C'} \mathbf{F} \cdot d\mathbf{r} = 0,$$



since the integral on C' is the negative of the integral on C .

Or more simply, consider the limiting case where C has been shrunk to a point; even as a point, it can still be considered to be the boundary of S . Since it has zero length, the line integral around it is zero, and therefore Stokes' theorem gives

$$\iint_S \text{curl } \mathbf{F} \cdot d\mathbf{S} = \oint_C \mathbf{F} \cdot d\mathbf{r} = 0.$$

6H-10 Let C be an oriented closed curve, and S a compatibly-oriented surface having C as its boundary. Using Stokes' theorem and the Maxwell equation, we get respectively

$$\iint_S \nabla \times \mathbf{B} \cdot d\mathbf{S} = \oint_C \mathbf{B} \cdot d\mathbf{r} \quad \text{and} \quad \iint_S \nabla \times \mathbf{B} \cdot d\mathbf{S} = \iint_S \frac{1}{c} \frac{\partial \mathbf{E}}{\partial t} \cdot d\mathbf{S} = \frac{1}{c} \frac{d}{dt} \iint_S \mathbf{E} \cdot d\mathbf{S}.$$

Since the two left sides are the same, we get $\oint_C \mathbf{B} \cdot d\mathbf{r} = \frac{1}{c} \frac{d}{dt} \iint_S \mathbf{E} \cdot d\mathbf{S}$.

In words: for the magnetic field \mathbf{B} produced by a moving electric field $\mathbf{E}(t)$, the magnetomotive force around a closed loop C is, up to a constant factor depending on the units, the time-rate at which the electric flux through C is changing.

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